

Public Utility Commission

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April 7, 2009

Via Electronic Filing and U.S. Mail

OREGON PUBLIC UTILITY COMMISSION ATTENTION: FILING CENTER PO BOX 2148 SALEM OR 97308-2148

RE: <u>Docket No. UM 1355</u> – In the Matter of THE PUBLIC UTILITY COMMISSION OF OREGON Investigation into Forecasting Forced Outage Rates for Electric Generating Units.

Enclosed for electronic filing in the above-captioned docket is the Public Utility Commission Staff's Opening Testimony.

/s/ Kay Barnes
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### PUBLIC UTILITY COMMISSION OF OREGON

#### **UM 1355**

# STAFF OPENING TESTIMONY OF Kelcey Brown

In the Matter of
THE PUBLIC UTILITY COMMISSION OF OREGON
Investigation into Forecasting Forced Outage Rates
for Electric Generating Units.

**April 7, 2009** 

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 100** 

**Opening Testimony** 

#### Q. PLEASE STATE YOUR NAME, OCCUPATION, AND BUSINESS

2 ADDRESS.

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- A. My name is Kelcey Brown. I am a Senior Economist in the Electric and Natural
- 4 Gas Division at the Public Utility Commission of Oregon. My business address
- is 550 Capitol Street NE Suite 215, Salem, Oregon 97301-2551.
- 6 Q. PLEASE DESCRIBE YOUR EDUCATIONAL BACKGROUND AND WORK
- 7 **EXPERIENCE.**
- 8 A. My Witness Qualification Statement is found in Exhibit Staff/101.
- 9 Q. WHAT IS THE PURPOSE OF YOUR TESTIMONY?
- 10 A. In this testimony I will discuss the Commissions current policy on the
- 11 calculation of not only forced outage rates, but the total calculation of
- 12 availability for electric generation units. I will provide my conclusions and
- recommendations regarding how the availability of an electric generation unit
- should be calculated for ratemaking purposes. In addition, I will make
- recommendations on the use of Industry data to be used as a benchmark when
- setting forced outage rates. I also recommend additional reporting
- 17 requirements for wind generation facilities.

#### Q. HOW IS YOUR TESTIMONY ORGANIZED?

- 19 A. I will first provide a brief summary of my conclusions and recommendations.
- 20 By way of background, I will describe the purpose of forced outage rates and
- 21 explain why the Commission recommended this docket be opened.
- I will organize the remainder of my testimony to address each of the issues in
- the Consolidated Issues List filed January 30, 2009. I also provide Exhibit

Staff/103-105 that details the statistical calculations and data that supports my recommendations.

### Q. PLEASE PROVIDE A BRIEF SUMMARY OF YOUR CONCLUSIONS AND RECOMMENDATIONS.

- A. After a thorough review of historical generation unit outage data I have reached the following conclusions:
  - I agree with the Commission's statement in Order No. 07-015 (UE-180)
     that the historical performance of the generating unit is the best predictor of what will occur in the future.
  - 2. I recommend that the formula used to calculate overall availability, and specifically forced outage rates, be changed. I will show that it is appropriate to separately calculate and model forced outage rates, planned outage rates, and a deferrable maintenance outage rate in order to accurately calculate availability for ratemaking purposes. I am defining a "forced outage" as an unplanned event that causes a generation facility to shutdown or reduce capacity immediately. "Planned outages" are outage events that are scheduled more than one year in advance. Finally, "maintenance outages" are outage events and reduced capacity events that are scheduled in a relatively short time frame (i.e. a few days to less than one year).
  - 3. I propose the use of industry data provided by the North American

    Electric Reliability Council (NERC) for benchmark purposes, in order to
    objectively define the level at which a plant has experienced an extreme

forced outage event, or on a cumulative basis, an extreme forced outage year. The definition of an extreme outage event generally refers to an extended time period, beyond what would be considered "normal." The benchmark will be set according to a discrete probability distribution of the industry outage information, with the benchmark set at less than 10 percent probability of occurrence. This tool will allow the Commission to objectively define whether the reported forced outage rate is reasonably likely to occur in the test period. If the benchmark shows that the rate is unlikely to occur in any given year, then an adjustment will be made to the forced outage rate.

- 4. The appropriate application of a forced outage rate on hydroelectric units, specifically storage hydroelectric units, should not cause an overall decrease in total MWh produced by the facility for the year. If a utility were able to show that a hydroelectric unit was forced to spill water in every occasion that it experienced a forced outage, then a decrease in total output would be appropriate; however, I have not found this to be the case.
- 5. Non-base load resources (e.g., gas fired peaking plants) require a different formula than that of base load resources (e.g., coal generation

<sup>&</sup>lt;sup>1</sup> A discrete probability distribution is a statistical term that means the description of a range of possible values (e.g. the forced outage rates of all reporting units) that a random variable (e.g. forced outage rate of a single unit) can attain, and the probability of that value falling within that range. For a graphical illustration of a probability distribution see Exhibit Staff/105, Brown/6. Stated differently, given the reported forced outage rates of 58 coal-fired generating units that are between 600-699 MW in 2007, the probability that a unit will incur a forced outage rate of greater than 10 percent has a less than 10 percent probability of occurrence, or is unlikely to occur.

ı	racilities). I propose the Commission use NERC's equivalent forced
2	outage rate (demand) (EFOR(d)) formula.
3	6. Finally, I propose the Commission require the utilities to provide a wind
4	availability report for each wind facility on an annual basis that will show
5	A. Maximum net output of the facility given the actual wind
6	conditions in a calendar year.
7	B. Lack of availability due to planned maintenance.
8	C. Lack of availability due to line loss.
9	D. Lack of availability due to forced outages, turbine failure, or non
10	scheduled maintenance.
11	E. Then, subtract factors B, C, and D above from A to provide the
12	actual capacity factor for a wind facility in a calendar year.
13	This information will provide a useful history that will allow the Commission
14	to obtain a better understanding of the different factors that affect the
15	actual output of wind facilities. For ratemaking purposes, this information
16	will provide an historical record that will facilitate a future determination of
17	the appropriate methodology for calculating the capacity factor of wind
18	farms in a test year.
19	
20	Forced Outage Rate Overview
21	Q. PLEASE PROVIDE A BRIEF DESCRIPTION OF FORCED OUTAGE
22	RATES AND EXPLAIN THEIR PURPOSE.

1 A. A forced outage is an unplanned failure that causes immediate shutdown of a 2 generating unit. Broadly speaking, the forced outage rate is calculated as a 3 proportion of forced outage hours to total hours that the unit is available for 4 operation. To calculate test period power costs for ratemaking, the 5 Commission uses a "forced outage rate" as part of the determination of 6 normalized generating unit availability. Since 1984, the Commission has used 7 a four-year rolling average of actual unit forced outage rates for a prediction of 8 what will potentially occur in the test period.

Q. ARE THERE OTHER OUTAGE EVENTS THAT ARE USED IN THE
CALCULATION OF AVAILABILITY OF A THERMAL GENERATION
PLANT?

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- 12 A. Yes. There are several types of outage events that are used in the overall 13 calculation of availability of a thermal generation facility. As stated in my 14 summary of conclusions, for simplicity I am defining them as: forced outage events (immediate shutdown or de-rate), maintenance outage events 15 16 (scheduled in a relatively short time frame, less than one year), and planned 17 outage events (scheduled in a time frame that is greater than one year). These 18 three generic descriptions are intended to capture all the outage events that a 19 generation facility will incur, and contribute to the calculation of its overall 20 availability.
- Q. PLEASE SUMMARIZE THE ISSUE OF FORCED OUTAGE RATES IN
  DOCKET UE 180, ORDER NO. 07-015.

A. In UE 180, Order No. 07-015, one of the issues before the Commission was
the treatment of the extreme outage events that occurred at the Boardman and
Colstrip coal plants. In UE 180, Staff and other intervening parties questioned
the four-year rolling average methodology and its ability to adequately account
for extreme events when calculating a future test year forced outage rate that
had a likely probability of occurrence.

#### Q. WHAT WAS STAFF'S RECOMMENDATION IN UE 180 FOR

#### **CALCULATING A FORCED OUTAGE RATE FOR THE TEST PERIOD?**

A. In UE 180, Staff recommended that Portland General Electric (PGE) discontinue using actual forced outage rates and instead use industry forced outage rate information provided by NERC, and the use of a standard peer group.<sup>2</sup> Staff concluded that the current methodology of a four-year rolling average assigned too much weight to recent extreme events, resulting in an unrealistic outage rate for the test period.

### Q. PLEASE SUMMARIZE THE COMMISSION DECISION IN ORDER NO. 07-015 (UE 180).

A. In relevant part, the Commission stated that it sought "...the most accurate forecast of forced outages at the relevant plants." The Order went on to say that "We continue to believe that past performance is the best predictor of a plant's outage rate." *Id.* In addition, the Commission concluded that the events that occurred at the respective plants were "extreme events" and directed that the associated hours be removed from the calculation of forced outage rates.

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<sup>&</sup>lt;sup>2</sup> See Order No. 07-015, page 14.

<sup>&</sup>lt;sup>3</sup> Ibid.

The Commission then ordered that a generic docket be opened to further investigate the currently-used forced outage rate methodology. UM 1355 is that docket.

#### Q. PLEASE EXPLAIN THE ORIGIN OF THE CURRENT COMMISSION

#### POLICY FOR CALCULATING OUTAGE RATES AND OVERALL

#### AVAILABILITY?

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A. In 1984, then-Commission Staff member Tom Harris proposed an equivalent outage rate methodology. This method took into account the different outage types (e.g. forced, maintenance, scheduled, and planned)<sup>4</sup> and used a four-year rolling average of actual plant performance in order to estimate what the equivalent outage rate of the plant would be for purposes of calculating power costs. Mr. Harris provided a formula for calculating the equivalent outage rates within each year.<sup>5</sup>

#### Q. IS THIS METHOD STILL EMPLOYED TODAY BY THE COMMISSION?

A. Yes. The original formula that was proposed by Staff witness Thomas Harris is still an integral part of a Utility's calculation of a generation facility's overall availability factor. However, each individual utility has some unique differences in how it applies this method to different types of generation facilities and how it models this calculation within a test year.

### Q. PLEASE PROVIDE SOME EXAMPLES OF THE DIFFERENCES BETWEEN EACH UTILITY.

<sup>4</sup> These outage types are not to be confused with my definitions provided previously.

<sup>5</sup> For a full copy of the 1984 Staff memo please see Exhibit Staff/102, Brown/1-21.

1 There are many differences between each utility. Four specific examples of 2 these differences are: 3 1. While Idaho Power does not model forced outages on its gas-fired 4 generation facilities, both PGE and PacifiCorp do; 5 2. In its last net variable power cost (NVPC) filing, PacifiCorp introduced a 6 forced outage methodology for some of its hydroelectric generation 7 facilities. No other utility models forced outages on its hydroelectric 8 generation units; 9 3. PacifiCorp uses a four-year rolling average in the calculation of a 10 planned outage rate for purposes of the test year. PGE and Idaho 11 Power forecast their planned outages in the test year, taking into 12 account specific maintenance that the utility is planning to perform; and 13 4. Until recently, PacifiCorp modeled a weekend/weekday split of its 14 outages, taking into account the ability of the operator to defer certain 15 outages to periods that have a lower economic impact on variable 16 power costs. 17 18 **Outage Rate Methodology** 19 Q. PLEASE REPRODUCE THE FORMULA FROM MR. HARRIS' 1984 MEMO. 20 A. Reproduced below is the formula that was recommended and approved in 21 1984, and is still in current use today:<sup>6</sup> EOR = FOH +EFOH + MOH + ESOH

<sup>6</sup> For a full explanation of the formula and definitions please review Exhibit Staff/102, Brown/5-7.

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SH + FOH + MOH

1 **EOR** = Equivalent outage rate – For our purposes this is the Forced outage 2 rate. 3 **FOH** = Forced outage hours – Time in hours during which a unit is unavailable. 4 **EFOH** = Equivalent forced outage hours – For a forced partial de-rate this is 5 the equivalent time in hours for a full forced outage. 6 **MOH** = Maintenance outage hours – The time in hours during which a unit is 7 unavailable due to a maintenance outage. 8 **ESOH** = Equivalent scheduled outage hours – The time in hours for a partial 9 maintenance de-rate. Scheduled outage hours and maintenance outage hours 10 are scheduled a relatively short time (i.e. a few days) in advance. These are 11 distinguished from planned outages, which are scheduled months or years in 12 advance. 13 **SH** = Service hours – The total number of hours that the unit was actually 14 operated with the breakers closed to the station bus. 15 16 Issue I.D: What forced outage rate methodology should the Commission 17 adopt for coal-fired generating plants? Q. PLEASE DISCUSS WHETHER YOU CONTINUE TO SUPPORT THE 18 19 CURRENTLY-USED COMMISSION FORMULA FOR CALCULATING 20 FORCED OUTAGE RATES. 21 A. I do not support the formula that the Commission currently uses for calculating 22 forced outage rates. As I will discuss in more detail, because of issues that the 23 Commission has faced in regard to planned outages, and observations of the 24 utility practice in scheduling maintenance outages during times that are 25 economically favorable, I am proposing the Commission adopt a new set of 26 formulas to be applied to all of the utilities participating in this docket. 27 Q. PLEASE SET FORTH YOUR RECOMMENDED FORMULAS. 28 A. I recommend the following three formulas (corresponding to three different 29 types of outages) for application to coal generation facilities:

FOR =	FOH + EFOH
	PH
MOR =	MOH + EMDH + EPDH
	PH
POR =	POH
	PH

Equivalent Availability Factor = 1- (FOR + MOR + POR)

**FOR** = Forced outage rate – This will continue to be modeled in the test year as it is currently done in the Utility's least-cost dispatch models.

**FOH** = Forced outage hours- The time in hours during which a unit is unavailable due to a forced outage.

**PH** = Period hours – Total hours in a calendar year, where the only variation would be a leap year versus a non leap year.

**MOR** = Maintenance outage rate – This will be the outage rate associated with deferrable maintenance. The application of this rate will differ from that of the forced outage rate, in test year modeling, to reflect actual plant history of occurrence within heavy load hours and light load hours. (I will discuss this further in testimony.)

**MOH** = Maintenance outage hours – The time in hours that a unit is unavailable due to a maintenance outage. These outages are scheduled in a relatively short time frame (i.e. a few days to a week) in advance.

**EMDH** = Equivalent maintenance de-rated<sup>7</sup> hours – An outage that requires a reduction in capacity, and is calculated as equivalent to the time in hours of a full forced outage event. These outages are scheduled in a relatively short time frame (i.e. a few days to a week) in advance.

**EPDH** = Equivalent planned de-rated hours – An outage that requires a reduction in capacity and is calculated as equivalent to the time in hours of a full forced outage event. These outages are scheduled in a short time frame (i.e. weeks to months) in advance. The planning period for these outages is longer than the EMDH, but shorter than the planned outage hours which are scheduled typically up to one year in advance.

**POR** = Planned outage rate – Will be modeled as a four-year rolling average of actual planned maintenance. This will be applied to the Utility's NVPC model and should be scheduled to occur during times that will realize the least impact on NVPC.

**POH** = Planned outage hours – The time in hours that a unit is scheduled to be unavailable due to annual planned maintenance. These outages are scheduled with a long lead time, typically greater than one year in advance.

<sup>&</sup>lt;sup>7</sup> The term "de-rated" refers to a reduction in the net available capacity of the unit. For example, assume a unit had a net available capacity of 100 MW, but due to a necessary maintenance the units net available capacity was reduced to 80 MW. This reduction in available capacity from 100 MW to 80 MW is referred to as a "de-rate." If this reduction in available capacity lasted five hours, than the calculated equivalent de-rated hours would be 20 MW \* 5 hours = 100 MWhs/100 MW = 1 hour of equivalent maintenance de-rated hours for the facility.

1 2 3 4		<b>Equivalent Availability Factor (EAF)</b> = This factor includes the effects of all outage events, and is equivalent to the percentage of time during which the unit was available for operation at full capability.
5		Maintenance Outages
6	Q.	WHAT IS THE DIFFERENCE BETWEEN A MAINTENANCE OUTAGE AND
7		A PLANNED OUTAGE?
8	A.	These two terms are very similar; however, they are very different in terms of
9		scheduling. The ability of a utility to schedule its outages is very important in
10		terms the impact that these outages have on power costs. Again, I am defining
11		a maintenance outage as an outage that is scheduled in advance in a relatively
12		short time frame, i.e. less than one year, and a planned outage is an outage
13		that is scheduled in advance in a time frame that is greater than one year.
14	Q.	PLEASE DISCUSS THE REASON FOR YOUR PROPOSED CHANGE IN
15		METHODOLOGY AND MODELING OF MAINTENANCE OUTAGES.
16	A.	On a modeled basis, in the test year, the current Commission method treats
17		maintenance outages the same as randomly occurring forced outages: it
18		evenly distributes them across all hours throughout the year. This modeling
19		method does not take into account the differences between a deferrable
20		maintenance outage and a forced outage, which necessitates immediate shut-
21		down of the unit.
22	Q.	WHEN A UTILITY SCHEDULES A MAINTENANCE OUTAGE, DOES IT
23		TAKE INTO ACCOUNT MARKET PRICES AND THE COST OF
24		REPLACEMENT POWER?

A. Yes. In Staff Data Request (DR) No. 5 each utility was asked to provide the actual occurrence of maintenance outage hours (MOH, EMDH, and EPDH) within high load hours<sup>8</sup> and within low load hours<sup>9</sup> over the last four known years. PacifiCorp provided the most comprehensive response, 10 which showed that on average for coal plants the occurrence of deferrable maintenance within high load hours was approximately 43 percent. The occurrence of deferrable maintenance during low load hours was 57 percent. The current methodology uses and evenly distributed calendar year, which has a ratio of high load hours to low load hours of 55 percent high load hours and 45 percent low load hours. Therefore, under the current Commission method customers are not realizing the benefit of the actual utility practice of scheduling the deferrable maintenance during times that have the least price impact.

#### Q. WILL THIS CHANGE IN MODELING CAUSE A DECREASE IN NVPC?

A. Yes. Changing the way that the utility currently models its maintenance outages will cause a decrease in NVPC. This change in modeling is appropriate because it will more accurately track the practice of the utility to schedule its maintenance during times that have the least impact on power costs.

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<sup>&</sup>lt;sup>8</sup> High Load hours refers to a frame of time during a 24 hour day when customer load and market prices are higher, i.e Monday through Saturday 6:00 am – 10:00 pm.

<sup>&</sup>lt;sup>9</sup> Low Load, or Light Load, hours refers to a frame of time during a 24 hour day when customer load and market prices are lower, i.e. Monday through Friday 10:00 pm – 6:00 am and Saturday 10:00 pm to Monday at 6:00 am.

<sup>&</sup>lt;sup>10</sup> See Exhibit Staff/103, Brown/1. This Exhibit includes a pivot table of the PacifiCorp provided data, which adds up the four years of reported data, shows only coal plants, and shows the ratio calculation of high load to low load hours.

I	Q.	15 II DIFFICULT FOR THE UTILITY TO TRACK THE OCCURRENCE OF
2		ITS OUTAGES ON AN ACTUAL BASIS DURING HIGH LOAD AND LOW
3		LOAD HOURS?
4	A.	No. The utility currently tracks and reports its maintenance events with a start
5		time and an end time. Once this time period is known, it is a simple calculation
6		to determine whether this period of time occurred during high load or low load
7		hours.
8	Q.	HOW DO YOU PROPOSE TO CALCULATE THE MAINTENANCE
9		OUTAGE RATIO OF HIGH LOAD TO LOW LOAD HOURS FOR
10		MODELING PURPOSES?
11	A.	Just as in the forced outage rate calculation, I recommend the use of a four-
12		year rolling average of the utility's actual history of maintenance outages that
13		occur during high load and low load hours.
14	Q.	HAVE ANY OF THE THREE UTILITIES EVER MODELED FORCED
15		OUTAGES TO TAKE INTO ACCOUNT SPECIFIC TIMES DURING THE
16		WEEK OR DAY?
17	A.	Yes. Until recently, within the last year, PacifiCorp calculated and modeled its
18		forced outages using a weekend/weekday split. This is an approach that
19		recognizes that if the utility has the ability to defer performing maintenance
20		activities, it will do so during times that have the least economic impact.
21	Q.	SHOULD YOUR PROPOSED MAINTENANCE CALCULATION AND
22		MODELING ALSO APPLY TO GAS-FIRED FACILITIES?

1	Α.	No. I will discuss later in testimony my proposal for modeling forced and
2		maintenance outages on gas-fired facilities.
3		
4		Issue IV. What methodology should the Commission adopted for planned
5		maintenance outages, and how should it be applied?
6	Q.	PLEASE DISCUSS YOUR PROPOSED METHODOLOGY IN
7		CALCULATING AND MODELING PLANNED OUTAGES IN A TEST YEAR
8	A.	The planned outage rate will be based on a four-year rolling average of the
9		utility's actual plant history. For ratemaking purposes this will allow planned
10		outage events, which can occur once every four to ten years, to conform to a
11		normalized test year.
12	Q.	IS YOUR PROPOSED METHODOLOGY FOR PLANNED OUTAGE RATES
13		CURRENTLY USED BY ANY OF THE UTILITIES IN THIS DOCKET?
14	A.	Yes. PacifiCorp currently uses a four-year rolling average of its planned
15		outages for modeling purposes.
16	Q.	IS IT APPROPRIATE TO ALLOW A UTILITY TO FORECAST ITS
17		PLANNED OUTAGES FOR PURPOSES OF A TEST YEAR?
18	A.	No. The Commissions ratemaking approach is to "normalize" a test year. This
19		means that events that only occur once every few years are not specifically
20		modeled; they are taken into account in calculating historical averages.
21		Therefore, it would be inconsistent with the Commission's approach to allow
22		the utility to forecast its planned outages, which are one-time events that may
23		vary widely from year to year.

Docket UM 1355

1	Q.	DO RECENT (	COMMISSION	<b>DECISIONS</b>	<b>CONTINUE</b>	<b>TO FAVOR</b>
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- 3 A. Yes. In UE 197, Fixed Plant Costs (Issue S-11), Staff proposed that the one-4 time maintenance costs associated with PGE's forecasted test year planned maintenance should be allocated over a ten-year period. 11 PGE agreed that 5 6 the maintenance was planned to occur only once every ten years, and was 7 willing to support a ten-year recovery period, which took into account the time 8 value of money. The Commission agreed with Staff's ten-year proposal and 9 supported PGE's recovery of the time value of money.
- 10 Q. IN LIGHT OF THE COMMISSION DECISION TO ALLOCATE FIXED COSTS ASSOCIATED WITH ONE-TIME MAINTENANCE EVENTS, 11 12 WOULD IT BE CONSISTENT TO ALLOW THE UTILITY TO MODEL ONE-13 TIME EVENTS IN THE TEST YEAR?
- A. No. 14
- Q. SHOULD YOUR PROPOSED PLANNED OUTAGE METHODOLOGY 15 16 ALSO BE APPLIED TO GAS-FIRED GENERATION FACILITIES?
- 17 A. Yes. The current practice of using a four-year average, and scheduling 18 planned outages during times that have the least economic impact, should also 19 apply to gas-fired facilities.

21 Issue I.F: What is the appropriate length for the historical period?

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<sup>&</sup>lt;sup>11</sup> See Order No. 09-020, page 23.

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#### 1 Q. WHAT WAS THE BASIS FOR THE CURRENT COMMISSION PRACTICE

2 OF USING A FOUR-YEAR ROLLING AVERAGE?

3 A. Mr. Harris explained his proposal of a 48-month period as follows: "The reason 4 I propose using a 48-calender month rolling average is that it reflects recent 5 plant experience, which I think tends to better portray expected operation over 6 the coming year. Four years of experience is sufficient to average out 7 variations and yet not include generally irrelevant experience from history long past." See Exhibit Staff/102, Brown/4. In addition, at the time of Mr. Harris' 8 9 memorandum PacifiCorp used a four-year planned maintenance cycle, which 10 further supported the use of the 48-calender month time period.

#### Q. DID YOU PERFORM A STATISTICAL ANALYSIS OF THE FOUR-YEAR 12 TIME PERIOD?

- A. Yes. I compiled the PacifiCorp outage data into energy lost by year and by plant, and attempted to find an underlying cyclical trend. I was unsuccessful in finding any statistically significant trend, including a four-year period, that was common among all of the generating facilities. 12
- Q. DID YOU TEST THE ABILITY OF OTHER TIME PERIODS TO MORE ACCURATELY PREDICT ACTUAL FORCED OUTAGES IN THE TEST YEAR?
- 20 A. Yes. Using plant information provided by PacifiCorp, I calculated rolling 21 averages using different time periods, i.e. 1 year, 2 years, 3 years, 4 years, 5

<sup>12</sup> See Exhibit Staff/104, Brown/1-4 for the forecasted trend analysis. I have included four examples of the trend analysis using the PacifiCorp coal-fired facilities Jim Bridger, Carbon, Dave Johnston and Hunter.

1 years, and 6 years, and a rolling average that applied different weights to more 2 recent years (i.e. 40%, 30%, 20% and 10%), as opposed to the current practice 3 of weighting each year evenly (i.e. 25%, 25%, 25%, 25%). Using a back-cast 4 comparison (forecasting for a year that has already occurred in order to 5 determine how accurate it would have been), I tested each methodology for 6 accuracy. 7 Q. WHAT DID YOUR RESULTS INDICATE? 8 A. My results indicated that a specific methodology in any given year may be the 9 most accurate, but in the next year, after incorporating new data, a different 10 methodology usually generated more accurate results. My overall conclusion 11 is that forced outage rates are random, and in that randomness there is no 12 definable pattern that can provide a statistical relationship that is greater than 13 the current methodology of a four-year average. 14 Q. DO YOU CONTINUE TO SUPPORT THE USE OF A FOUR-YEAR 15 ROLLING AVERAGE FOR PURPOSES OF CALCULATING FORCED 16 **OUTAGE RATES?** 17 A. Yes. Based on the lack of finding a statistically significant method that 18 produces more accurate results than the existing practice, I find no reason to 19 recommend a change from the current practice of using a four-year rolling 20 average with equal weighting. 21 22 Issue I.B. and I.C: Should extreme events be included in the forced 23 outage rate determination?

I	Q.	WHAT IS YOUR RECOMMENDATION FOR THE TREATMENT OF
2		EXTREME EVENTS IN FORCED OUTAGE RATES?
3	A.	For extremely long events, and for years that a unit experiences a significant
4		number of small outages that is outside what would be considered normal, I
5		propose that the Commission use NERC outage rate information as a
6		benchmark to determine whether the forced outage rate for the test period is
7		reasonable and likely to occur.
8	Q.	IS IT A COMMON PRACTICE FOR THE COMMISSION TO USE
9		BENCHMARKS AS A TEST OF REASONABLENESS?
10	A.	Yes. Most recently, in UE 200 PacifiCorp's Renewable Adjustment Clause,
11		Staff utilized benchmark data to determine whether PacifiCorp's costs for its
12		proposed wind generation facilities were reasonable as compared to industry
13		data.
14	Q.	PLEASE EXPLAIN YOUR PROPOSAL TO USE NERC INDUSTRY
15		FORCED OUTAGE RATE INFORMATION AS A BENCHMARK FOR
16		EXTREME EVENTS.
17	A.	I am proposing to use NERC generating unit-level information, categorized by
18		year, fuel type and size, to determine whether the calculated forced outage
19		rate for the test period is reasonable and falls within the range of data that is
20		statistically likely to occur. Exhibit Staff/105, Brown/1-5, shows forced outage
21		rate information for four categories of coal-fired units: 600-699 MW, 500-599
22		MW, 400-499 MW, and 300-399 MW for the years 1999 through 2007.

#### Q. PLEASE DISCUSS HOW YOU USED THIS INFORMATION TO

2 DETERMINE A BENCHMARK.

A. Using the annually reported forced outage rate for each unit, I calculated a discrete probability distribution. Simply, this means that the range of possible values is contained to the reported rates for that year, i.e. the lowest rate reported and the highest rate reported sets my lower and upper limits. I calculate a greater than 90<sup>th</sup> percentile value probability of occurrence and a less than 10<sup>th</sup> percentile value probability of occurrence. This means that for the 57 coal-fired units with a rated capacity of 600-699 MW reporting in 1999, 90 percent of the time a reported forced outage rate is going to be less than 13.41 percent. At the other end of the spectrum, the likelihood that the rate will be less than 1.96 percent has a less than 10 percent chance. I performed this calculation for each year and then used these 90 and 10 percent values to calculate a four-year rolling average which will be used as the benchmark in the test year.<sup>13</sup>

### Q. WHY IS IT NECCESARY TO HAVE BOTH A 90<sup>TH</sup> PERCENTILE VALUE AND A 10<sup>TH</sup> PERCENTILE VALUE?

A. In terms of parity, it is important to note the probability of occurrence from both sides of the mean. This is the same concept as having a true-up mechanism in NVPC, which takes into account the possibility of over-forecasting and of under- forecasting NVPC.

<sup>&</sup>lt;sup>13</sup> All calculations are at the bottom of each category, by capacity, in Exhibit Staff/105, Brown/1-5.

1	Q.	HOW DO YOU PROPOSE THE COMMISSION UTILITIZE THESE 90
2		PERCENTILE AND 10 <sup>TH</sup> PERCENTILE VALUES AS A BENCHMARK?
3	A.	The Commission should use the NERC data to determine whether a utility's
4		reported forced outage rate is likely to occur within the test year. If the utility
5		forced outage rate is larger than the 90 <sup>th</sup> percentile probability of occurrence,
6		then according to industry statistics it is unlikely to occur within the test period.
7		The appropriate action would be to adjust the utility forced outage rate to within
8		the likelihood of occurrence, at the 90 <sup>th</sup> percentile value.
9	Q.	WOULD THE SAME ADJUSTMENT BE MADE FOR THOSE VALUES
10		THAT FALL BELOW THE 10 <sup>TH</sup> PERCENTILE PROBABILITY OF
11		OCCURRENCE?
12	A.	Yes. It stands to reason that if the Commission recognizes that there are years
13		that may be unusually bad, then they must also take into account those years
14		that are unusually good.
15	Q.	ONCE THIS ADJUSTMENT WAS MADE WOULD FURTHER
16		COMMISSION ACTION BE NECESSARY?
17	A.	No. If a utility believed it needed to recover additional power cost expenses,
18		above what its expected rate of return is, then it has the option to file for a
19		deferral of power cost expenses that it alleges were unreasonably high due to
20		unforeseen events. In addition, PGE and Idaho Power have in place a true-up
21		mechanism that allows the utility to recoup those costs that are above or below
22		its forecasted NVPC (after the application of a deadband and an earnings
23		review) on an annual basis. This type of mechanism further justifies the need

to have a more accurate forecast of what will likely occur within the test period,
rather than the current four-year rolling average method that effectively
provides the utility with a retroactive ratemaking tool.

# Q. HAVE YOU CONSIDERED THE TREATMENT IN UE 180, WHERE THE COMMISSION REMOVED THE TIME PERIOD OF THE OUTAGE FROM BOTH THE DENOMINATOR AND THE NUMERATOR OF THE FORCED OUTAGE RATE CALCULATION?

A. Yes. I have. In UE 180, and in other rate cases, the Commission's decision to remove the extreme outage period from the calculation has the effect of giving greater significance to those events left in place, and thus results in a relatively higher forced outage rate. For example:

	Year 1	Year 2	Year 3	Year 4	Rolling Average
Total forced outage hours	60,000	100,000	50,000	400,000	610,000
Total MWH in one year	876,000	876,000	876,000	876,000	3,504,000
Forced outage rate	7%	11%	6%	46%	17%
Commission	decision in yea	ar four, remove	es 300,000 ho	ours from ou	itage calculation
		37. 2	\/ A	Voor 4	
	Year 1	Year 2	Year 3	Year 4	Rolling Average
Total forced outage hours	<b>Year 1</b> 60,000	<b>Year 2</b> 100,000	<b>year 3</b> 50,000	100,000	Rolling Average 310,000
Total forced outage hours Total MWH in one year					

As is shown, the remaining 100,000 hours in Year 4 now calculates as a 17 percent forced outage rate, while in Year 2 for the same amount of outage hours this only calculates as an 11 percent outage rate. The NERC-benchmark approach is a superior method of accounting for the type of situation addressed in UE 180.

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Issue I.A: Different Forecasting Method for a Peaker Plant versus a Base

3 Load Plant?

4 Q. SHOULD THERE BE A DIFFERENT FORECASTING METHODOLOGY

FOR A GAS-FIRED PEAKING FACILITY VERSUS A BASE LOAD COAL-

FIRED FACILITY?

- 7 A. Yes. Mr. Harris did not address gas-fired facilities in his 1984 memo. The 8 utilities have used the same methodology for gas-fired plants as for coal-fired 9 plants, but to date the Commission has not required such an approach. Gas-10 fired peaking facilities have very different operating schedules than a base load 11 coal-fired facility. The time of day that a peaking plant runs and the amount of 12 time that it will run as opposed to a coal plant is significantly different. The 13 current method of calculating forced outages rates for peaking facilities 14 significantly under- or over-states the availability of the unit, and leads to 15 incorrect modeling.
- 16 Q. PLEASE PROVIDE AN EXAMPLE OF WHY THE CURRENT METHOD
  17 CAN LEAD TO INCORRECT MODELING.
  - A. For example, in a calendar year if a gas-fired peaking facility was called to run nine times, it would then have nine expected start times. If in one of those times it did not start, the utility would then assume a length of time that the unit would have run, and record this as forced outage hours. From a reliability perspective the unit only failed one out of nine times, which, if calculated as a forced outage rate is 11 percent. However, if during these nine start times the

facility ran, or was expected to run, a total of 270 hours, and during the one 2 outage event it was expected to run 60 hours, the calculated forced outage rate 3 would be: 60/270 = 22%. For a 100 MW facility, it would be modeled as only 4 available to provide power up to 78 MW for the test year.

#### Q. WHAT IS YOUR PROPOSAL THAT WILL BETTER CALCULATE A FORCED OUTAGE RATE OF A GAS-FIRED PEAKING FACILITY?

A. A method prescribed by NERC, called equivalent forced outage rate demand (EFOR(d)), takes into account the number of attempted starts, the number of actual starts, and the average forced outage duration. This formula will provide a more accurate calculation of forced outage rates, and subsequently more accurate modeling of these facilities in the test year.

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#### Issue I. E: New Thermal Resources

#### Q. HOW SHOULD NEW THERMAL RESOURCES BE TREATED?

As prescribed in the 1984 Memorandum, the appropriate methodology for a new resource, with less than four years of actual plant performance data, should use NERC industry data to substitute for those years, until such time that four years of actual information becomes available. The NERC industry information should be incorporated according to fuel and capacity rating, with the average forced outage rate for that category substituted for the applicable years.

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#### Issue I.G: Non-Outage Related Adjustments

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1	Q.	SHOULD NON-OUTAGE RELATED ADJUSTMENTS BE INCLUDED IN
2		THE FORCED OUTAGE RATE DETERMINATION?
3	A.	I am unaware of any non-outage related adjustment that may be appropriate to
4		include in the forced outage rate determination. I am unable to make a
5		definitive statement on this issue until participants in this docket have had an
6		opportunity to cite examples of such non-outage events.
7		
8		Issue I.H: New Capital Investment
9	Q.	SHOULD THE FORCED OUTAGE RATE BE ADJUSTED WHEN NEW
10		CAPITAL INVESTMENT IMPROVES RELIABILITY?
11	A.	If the utility entered into an agreement with an outside party, in which it was
12		guaranteed a quantified increase in reliability in a particular plant through new
13		capital investment, subject to liquidated damages or other compensation, then
14		it would be appropriate to reflect the guaranteed increase in reliability for the
15		forecasted test year. Outside these conditions it would be difficult for the utility
16		to accurately forecast an increase in reliability due to capital investment.
17		
18		Issue II: Hydro Availability Method
19	Q.	HAS THE COMMISSION ADOPTED A HYDRO AVAILABILITY
20		METHODOLOGY?
21	A.	Currently, the Commission does not have an adopted hydro availability model.
22		Utilities are not currently required to report incidents of forced outages on hydro

facilities to NERC. The definition of a forced outage incident for a hydro facility

and the subsequent consequences of that outage are very different from that of a thermal facility. For example, if a coal-fired base load facility experiences a forced outage it loses the ability to produce that power. However, when a hydroelectric facility experiences a forced outage, the water is still behind the dam and will be used for generation at another time. The total production of the hydroelectric facility will not decrease for the year due to forced outages.

### Q. DO PGE, IDAHO POWER, OR PACIFICORP CURRENTLY MODEL FORCED OUTAGES FOR THEIR HYDRO FACILITIES?

A. PacifiCorp is the only utility that has introduced forced outages for hydro facilities, which impacts hydro availability within its NVPC model.

### Q. PLEASE DESCRIBE PACIFICORP'S FORCED OUTAGE METHODOLOGY AS IT PERTAINS TO HYDRO FACILITIES.

A. In UE 199, PacifiCorp proposed through its Transition Adjustment Mechanism filing (TAM) to include forced outages for specific hydro facilities (storage facilities). At that time, PacifiCorp utilized its Vista model to generate a weekly amount of MWh of hydro availability, which it then input into its NVPC dispatch model (GRID). GRID then took the total MWh of energy and dispatched it according to its least cost dispatch logic. The Vista model uses a monthly four-year average of "forced outage hours" from these specific storage facilities.

Once the average number of forced outage hours per month is known, specific time periods within that month are selected as "unavailable." For example, in the month of April, if the average number of hours of forced outages is 50 then

1		specific time periods, e.g. Monday, Tuesday and Wednesday in the second
2		week of April, are unavailable to the model for generation.
3	Q.	IS THIS METHODOLOGY CONSISTENT WITH THE PRINCIPLE OF A
4		STORAGE HYDRO FACILITY WHICH STORES ENERGY BEHIND A
5		DAM?
6	A.	No. While I acknowledge that hydro facilities are not always going to be
7		available when they are called upon, it is incorrect to use a method that does
8		not take into consideration the fact that the hydro facility retains its ability to
9		generate that power in the future. Unless the utility is required to spill the water
10		due to biological constraints or other mitigating factors, and the energy
11		capability is lost, the utility should not reflect a lower production of power from a
12		storage hydro facility due to forced outages.
13	Q.	HAS PACIFICORP PROVIDED AN EXAMPLE WHEN IT WAS REQUIRED
14		TO SPILL STORED WATER RELATED TO A FORCED OUTAGE?
15	A.	No.
16	Q.	DOES STAFF PROPOSE A METHODOLOGY FOR FORCED OUTAGES
17		ON HYDRO FACILITIES?
18	A.	No. Storage hydro facilities present their own parameters of operations, which
19		current thermal forced outage rate methodologies do not adequately address.
20		
21		III: What wind availability reporting method should the Commission
22		adopt?

Docket UM 1355

1	Q.	PLEASE DISCUSS YOUR RECOMMENDATION OF AN ANNUAL WIND
2		AVAILABILITY REPORT, TO BE FILED BY EACH UTILITY THAT OWNS
3		AND OPERATES A WIND FACILITY.
4	A.	I propose that the Commission require the utilities to provide a wind availability
5		report for each wind facility that it owns and operates that will show:
6		A. Maximum net output of the facility given the actual wind conditions in
7		a calendar year;
8		B. Lack of availability due to planned maintenance;
9		C. Lack of availability due to line loss;
10		D. Lack of availability due to forced outages, turbine failure, or non-
11		scheduled maintenance; and,
12		E. Factors B, C, and D will be subtracted from A, to provide the actual
13		capacity factor for a wind facility in a calendar year.
14	Q.	WHY WILL THIS INFORMATION WILL BE USEFUL TO THE
15		COMMISSION?
16	A.	This information will provide an account of the history of the wind farm, allowing
17		the Commission to obtain a better understanding of the different factors that
18		affect the actual output of wind facilities. For ratemaking purposes, this
19		information will provide an historical record that will facilitate a determination, in
20		the future, of the appropriate methodology of calculating the capacity factor of
21		wind farms in a test year.
22		

Docket UM 1355

- 1 <u>Issue V: What data reporting requirement should the Commission require</u>
- 2 <u>regarding outages?</u>
- 3 Q. DO YOU PROPOSE ANY ADDITIONAL DATA REPORTING
- 4 REQUIREMENTS AT THIS TIME FOR GENERATING FACILITIES OTHER
- 5 **THAN WIND FARMS?**
- 6 A. No.
- 7 Q. DOES THIS CONCLUDE YOUR TESTIMONY?
- 8 A. Yes.

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 101** 

**Witness Qualification Statement** 

#### WITNESS QUALIFICATION STATEMENT

NAME: Kelcey Brown

EMPLOYER: Public Utility Commission of Oregon

TITLE: Senior Economist, Electric and Natural Gas Division, Resource and

Market Analysis

ADDRESS: 550 Capitol Street NE Suite 215, Salem, Oregon 97301-2115.

EDUCATION: All course work towards Masters in Economics

University of Wyoming

B.S. University of Wyoming

Major: Business Economics

Minor: Finance

EXPERIENCE: Since November 2007 I have been employed by the Public Utility

Commission of Oregon. Responsibilities include research, analysis and recommendations on a wide range of cost, revenue and policy issues for electric utilities. I have provided testimony in UE 199 and LE 200, and actively portion to the regulatory proceedings in

UE 200, and actively participated in regulatory proceedings in

Oregon, including UE 195, UE 198, and UM 1355.

From June 2003 to November 2007 I worked as the Economic Analyst for Blackfoot Telecommunications Group, a competitive and incumbent telephone provider in Missoula, Montana. I conducted all long and short term sales and revenue forecasts, resource acquisition costbenefit analysis, business case analysis on new products and buildouts, pricing, regulatory support, market research, and strategic planning support.

From May 2002 to August 2002 I worked as an intern at the Illinois Commerce Commission in Springfield, Illinois. I performed competitive market analysis, spot market monitoring and pricing review, and extensive research on locational marginal pricing and transmission system incentives for development.

My course work, towards a Master's degree at the University of Wyoming, focused heavily on the regulatory economics of network industries such as electricity, natural gas, and telecommunications.

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 102** 

**Exhibits in Support of Opening Testimony** 



#### PUBLIC UTILITY COMMISSIONER OF OREGON

LABOR & INDUSTRIES BUILDING, SALEM OREGON 97310 PHONE (503) 378-6053

July 31, 1984

Mr Larry A Crowley
Asst Manager-Rates
Idaho Power Company
Box 70
Boise ID 83707

Mr Grieg L Anderson
General Manager
Rates & Revenue Requirements
Portland General Electric Co
121 SW Salmon St
Portland OR 97204

Mr David W Sloan, Manager Rates & Regulations Pacific Power & Light Co 920 SW Sixth Ave Portland OR 97204

277 - 1 1384

PATER REPORT

Earlier this year, we had extensive discussions concerning the performance of several thermal plants as used in setting rates. As a result of those discussions, Tom Harris has authored the attached memorandum stating staff's position on these matters.

For rate-making, we will use historical plant data to calculate the production available from each thermal plant. In general, we will use 48 calendar months, on a rolling basis, of unit performance data. Definitions and procedures are discussed in the attached memo.

As part of our engoing rate-making process, we will need routine reports from each utility on the performance of thermal units. The PUC staff is attempting to treat thermal plants uniformly from plant to plant and company to company. The request for specific thermal plant data is directed to each utility as listed.

Idaho Power

-Valmy 1-2

Portland General Electric

-Trojan Boardman Colstrip 3-4 ~

Pacific Power & Light

-Jim Bridger 1-4
Dave Johnston 1-4
Wyodak
Centralia 1-2
Colstrip 3-4

#### Data Request

For Trojan, PGE is to continue providing staff with the monthly operating data report and the semiannual net electric generation graph.

July 31, 1984 Page Two

For all the other plants, within 30 days after the end of each month, each company, as listed above, is to provide the PUC staff the following data for the preceding month for each thermal unit.

Month, Year
Plant and Unit Name
Maximum Dependable Capacity
Forced Outage Hours
Maintenance Outage Hours (Short Notice)
Planned Outage Hours (Annual Outage)
Reserve Shutdown Hours
Period Hours
Service Hours
Equivalent Schedule Outage Hours
Equivalent Forced Outage Hours
Gross Generation—mwh
Net Generation—mwh
Planned Maintenance Schedule for Current and
Subsequent Year

The above data is to be provided for the preceding month, year-to-date, preceding 12 calendar months, and 48 calendar months. Except for the last item in the list, all the other data is contained in the attached example Unit Data Summary report. Also, we wish to begin receiving the semiannual net electric generation graph for each plant as listed above for your company. In addition, you will note that performance data for Colstrip 3 depart from that used in the tracking filing. We propose using the technique suggested in Tom's memo for that facility in future rate reviews. Finally, Page 3 of Appendix A of the attached memo contains a reference to the North American Electric Reliability Council (NERC). We ask that each year each company foward the annual report from NERC containing such information immediately upon receipt.

Some additional specific questions regarding certain of the thermal plants will be transmitted in another letter.

If you have questions about this request, please contact Roger Colburn at 378-6894. Incidentally, Scott Girard has assumed responsibilities previously held by Tom Harris. His number is 378-6625.

William G. Warren

Manager

Energy Division

ger/05611

Attachments ·

cc: Roger Colburn Scott Girard

150

PACIFIC POWER & LIGHT COMPANY UNIT DATA SUNNARY PERIOD 5/ 1/83 THRU 4/30/84 WYODAK UNIT 1

FIRST SYNCHROHIZED 6/ 8/78 14:21	RONIZED 67 8		NAMEPLATE= 332MW	DECLARED COMMERCIAL	AL 9/18/78	178	
	. •	48 MONTH TOTAL	OTAL PERIOD	D YEAR TO DATE		LAST MONTH	1
FORCED	(HOURS/#)	712.10/	77 48.58/	5 5.28/ I	. 0	0.00.0	
MAINTENANCE	(HOURS/#)	29.95/	2 0.00/	0 0.00%		0 .00.0	
PLANNED	(HOURS/#)	2649.38/	6 893.83/	2 0.00/ 0		0.00.0	
RESERVE SHUTDOWN	(HOURS/#)	/00.0	/00.0	0 /00.0 0		0 /00.0	
FORCED PARTIAL	(HOURS/#)	1999.37/ 2 2079.65	222 67.287 67.28	16 3.28/ 2 3.28	200	2.40 1	
SCHEDULED PARTIAL	(HOURS/11)	127.12/	16 0.00/	0 /00.0 0		0.00.0	_
NONGURTAILING- EQUIPMENT-	ENT_CHOURS/#)	64,42/6	/00.09	004000	J 0.	0.00%	_
PERIOD	CHOURS	35064.00	8784.00	2904.00	720.00	. 00	
SERVICE	(HOURS)	31672.57	7841.58	2898.72	720.00	0.0	
AVAILABILITY	(HOURS)	31672.57	7841.58	2898.72	720.00	0.0	
EQUIVALENT SCHEDULED	(HOURS)	50.82	00.0	00.0	•	0.00	
EQUIVALENT FORCED	(HOURS)	335.70	14.58	0.56		0.45	
GROSS GENERATION	(MUH)	10230363.00	2512312.00	1044414.00	260368,00	0.0	
NET GENERATION	CMMHO	9270850.00	2283622.00	956340.00	237962.00	00	
MAX. DEPEND. CAP. GROSS	ISS (MM)	345.00	345.00	345.00	345.00	0.0	
UNIT YEARS		4.00	1.00	0.33	0.	. 80.0	

NOTE: EFFECTIVE SEPTEMBER 1,1977 THE UNIT MDC WAS CHANGED FROM 345 TO 345 POURS PARTIAL DUTAGE DATA INCLUDES HONCONCURRENT (UPPER) AND CONCURRENT OUTAGE HOURS

(C: MCLAGAN, MORGAH, UDY, VINCENT, GENERATION ENGINEERING, POWER RESOURCES, THERMAL OPERATIONS

## PUBLIC UTILITY COMMISSIONER OF OREGON INTER-OFFICE CORRESPONDENCE

(NOT FOR MAILING)

DATE:

July 18, 1984

TO:

Bill Warren .

FROM:

Tom Harris

SUBJECT: Thermal Plant Performance

#### INTRODUCTION

In this memo I shall summarize my investigation and analysis of the performance of thermal plants for use in our rate-making process. This memo represents a "final" wrap-up of the plant performance project I began in 1983. My purpose is to develop reasonable methods for calculating thermal plant performance levels to be used for calculating the cost of power.

Performance level includes both month-to-month availability of, or net megawatts available from, each plant and the length of the expected annual maintenance period. I intend to propose a method for calculating performance that can be applied uniformly from plant to plant and from company to company. There is an exception. I shall treat Trojan a little differently because PGE collects data for Trojan to meet NRC requirements, and such data differs from that collected for coal fired plants.

In general, I propose to use a 48-calendar month rolling average of historical performance for each thermal unit on which to base cost of power calculations. The megawatts available from each thermal unit are to be calculated by (1.0 - EOR) \* (MW Net) for the months during the year the unit is scheduled to be available. Definitions for Equivalent Outage Rate (EOR), MW Net, Maximum Dependable Capacity (MDC), and other terms and procedures will be discussed later in this memo. EOR is to be calculated for a 48-month period for most thermal units. The reason I propose using a 48-calendar month rolling average is that it reflects recent plant experience, which I think tends to better portray expected operation over the coming year. Four years of experience is sufficient to average out variations and yet not include generally irrelevant experience from history long past.

#### **DEFINITIONS**

The definitions and procedures I am using are intended to be similar to those adopted by the Edison Electric Institute and the North American Electric Reliability Council. The differences I propose adopting were suggested by Pacific Power & Light and by Idaho Power Company.

Bill Warren July 18, 1984 Page Two

Following I shall list and illustrate the formula and definitions to be used.

MW available = (1.0 - EOR) \* (MW Net)

SH + FOH + MOH + ESOH

MW Net = MDC \* Net Generation mwh
Gross Generation mwh

- EA Equivalent Availability Includes effects of EOR and planned maintenance. Essentially equivalent to the percentage of time during which the unit was available for operation at full capability.
- EOR Equivalent Outage Rate EOR categorizes and summarizes equipment failures and their corresponding outage periods. EOR characterizes the inability of a unit to operate when required for service. It essentially is equivalent to percentage of an anticipated service, during which a unit was not available for operation at full capability. Time required for planned outages and economy or reserve shutdowns is excluded when computing this index.
- EFOH Equivalent Forced Outage Hours For a partial forced outage reduction, EFOH is equivalent time in hours for a full forced outage which would equal mwh lost because of the partial outage.
- ESOH Equivalent Scheduled Outage Hours For a partial scheduled outage, ESOH is equivalent time in hours for a full scheduled outage which would equal mwh lost because of the partial outage.

<u>Scheduled and maintenance outages</u> are scheduled a relatively short time (i.e., few days) in advance. They are distinguished from planned outages which are planned months in advance (i.e., annual outages).

- Forced Outage The occurrence of a component failure or other conditions which requires that the unit be removed from service immediately or up to and including the very next weekend.
- Forced Partial Outage The occurrence of a component failure or other conditions which requires that the load on the unit be reduced two percent or more immediately or up to and including the very next weekend.
- FOH Forced Outage Hours The time in hours during which a unit is unavailable due to a forced outage.

Bill Warren July 18, 1984 Page Three

- FPOH Forced Partial Outage Hours The time in hours during which a unit is unavailable for full load due to a forced partial outage.
- MOH Maintenance Outage Hours The time in hours during which a unit is unavailable due to a maintenance outage.

A maintenance outage or scheduled outage is scheduled a relatively short time (i.e., few days) in advance. For our purposes, a maintenance outage is treated like a forced outage.

- PH Period Hours Hours in the period under consideration, usually one month, one year, or four years.
- POH Planned Outage Hours The time in hours a unit is unavailable due to a planned outage.

Planned outages are planned months in advance. Generally these are annual maintenance outages.

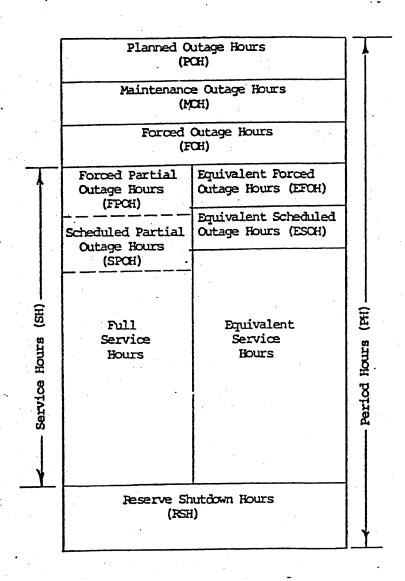
- POR Partial Outage Reduction The size of reduction from MDC in megawatts during a partial outage.
- RSH Reserve Shutdown Hours The time in hours a unit is shutdown for economy reasons.
- SH Service Hours The total number of hours the unit was actually operated with breakers closed to the station bus.
- SPOH Scheduled Partial Outage Hours The time in hours during which a unit is unavailable for full load due to a scheduled partial outage. Scheduled partial outages are generally scheduled a short time in advance. For our purposes, they are treated like a forced partial outage.
- mw Megawatts
- MDC Maximum Dependable Capacity The dependable main-unit capacity, winter or summer, whichever is smaller. MDC includes station use.
- MW Net Megawatts Net Net megawatts available from a unit or plant excluding station use. For our purpose here:

MW Net = MDC \* Net Generation mwh
Gross Generation mwh-

Figure 1 on the next page illustrates some of the above terms.

For our purposes, I have specified different definitions for and uses of the terms planned outage, maintenance outage, and scheduled outage than we have commonly used in the past. Maintenance outages or

Figure 1
Thermal Unit Availability Statistics
Definitions



Bill Warren July 18, 1984 Page Four

scheduled outages are interchangeable terms. They both refer to unit outages which are scheduled or known a relatively short time in advance, i.e., a few days. These outages are treated like forced outages.

A planned outage is known months in advance. This outage is usually the annual maintenance shutdown. Planned outages are to be specifically used in rate-making cost of power calculations by showing a unit as being out-of-service. Planned outages are not reflected in calculations for the Equivalent Outage Rate (EOR).

## **PROCEDURES**

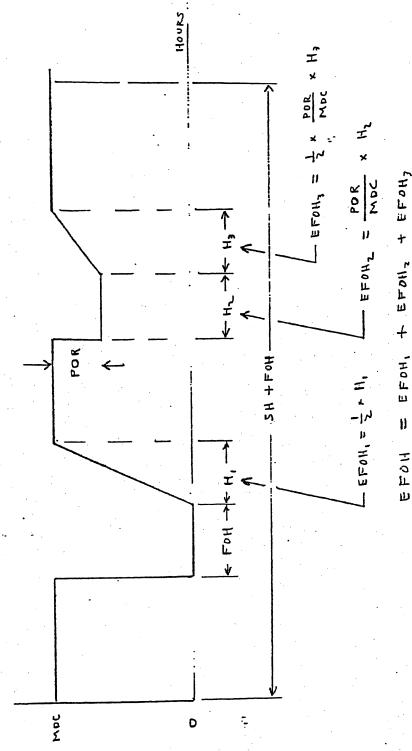
For rate-making cost of power calculations the mw available for each thermal unit are to be calculated as indiciated earlier, that is mw available = (1.0 - EOR) \* (MW Net). A plant's mw available is the sum of all units' mw available. Utilities may aggregate several thermal units at one site into a plant for rate-making purposes.

The megawatts available from thermal units for rate making will generally be less than megawatts used by the utilities for Coordination Agreement purposes. The reason is the agreement permits utilities to inflate, within limits, the expected average megawatts available from the thermal plants. On average, it is to the benefit of the utilities and their ratepayers to do so. Utilities can borrow amounts of energy from the Northwest hydro system based on the firm energy resources which they report they have available. The utilities gamble that they can repay the borrowed energy from future hydro energy. In poor hydro years, they must repay energy from their thermal resources.

The procedures for calculating EFOH and ESOH are illustrated on the following two pages. The procedures are alike. It can be seen that EFOH and ESOH are the sum of equivalent outage hours for several partial forced or partial scheduled outages.

The EOR and MW Net are to be calculated using the most recent available 48-calendar months of performance data for each thermal unit. For thermal units with less than 48 months operation, i.e., Colstrip #3 and Valmy, the Equivalent Outage Rate to be used will be the weighted (by number of months) average of actual historical performance and national averages. The national averages I will use are shown on page 3 of Appendix "A." Those averages were compiled and published by the Thermal Resources Committee of PNUCC. The source of data is the North American Electric Reliability Council (NERC). Members of the Thermal Resources Committee include representatives of several Northwest utilities, including Portland General Electric and Pacific Power & Light. The numbers shown in the appendix are illustration only. I expect the utilities to annually furnish updated data reflecting national average performance of new thermal plants.

An example: If PGE files for a rate increase when Colstrip is two years old, PGE will have 24 months of historical data. Obviously, we will not know what the EOR for Colstrip #3 will be in its third

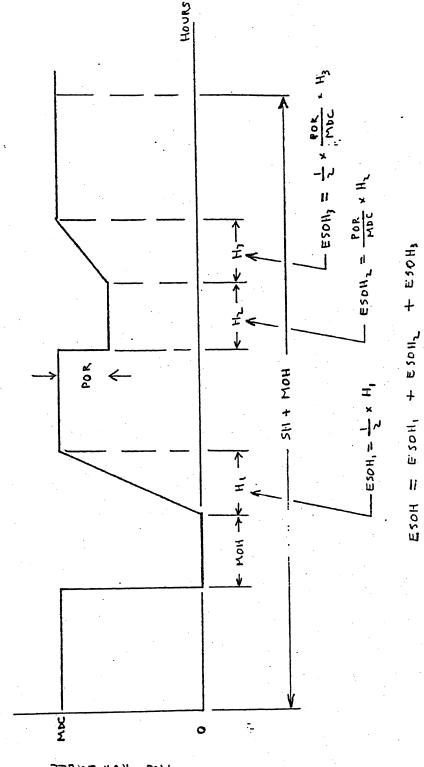


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year. From the appendix we see the national average Forced Outage Rate for coal units of Colstrip's approximate size for the third year of operation is 12.3 percent. I shall use Forced Outage Rate, which differs slightly from EOR, for new plants because that is the data available from the PNUCC. However, we need to give some consideration to Colstrip's two years of actual operation. Let us assume the EOR for two years is actually 16.0 percent. The weighted (by number of months) average of 24 months at 16.0 percent and 12 months at 12.3 percent is 14.8 percent.

Therefore, the estimated EOR for Colstrip #3 for that coming year would be 14.8 percent. The mw available will be (1.0 - 0.148) \* (700 mw) = 596.4 mw for the unit. PGE should show their 20 percent share as 119 mw for the approximate 11 months per year Colstrip #3 is scheduled to be on line.

A utility may use, for rate-making purposes, the same equivalent outage rate and planned maintenance schedule that it uses for the Coordination Agreement. I suggest that if a utility cannot provide adequate data, calculations, and workpapers to support lower performance levels (higher EOR or lower annual availability), then the PUC staff should seriously consider using Coordination Agreement values.

The MW Net calculation is to be used to reflect station use. That is, MW Net excludes station use. In power cost calculations, station use should not be a separate line item nor added to system load. I shall calculate MW Net as indicated earlier, that is:

MW Net = MDC \* Net Generation mwh
Gross Generation mwh

Portland General Electric includes in their power cost calculations a line item called non-running station service. That item is effectively a load. It is correct to use only for months a unit is planned to be off line, i.e., during planned annual maintenance. For months the unit is planned to be in service, station use is incorporated in the MW Net calculation. An alternative, which I prefer, is to have net generation mwh reflect energy used by a thermal unit when it is shutdown. In that case, non-running station service must not be specifically included in power costs.

The annual planned maintenance for rate making for each unit should be an average of a four-year cycle actual planned outages. The reason I chose a four-year average is that actual planned outages run different numbers of days from what was scheduled during the previous year. In actual practice, utilities vary from the previously scheduled outage dates in response to operating conditions.

Utilities normally expect to have relatively short planned outages for three years out of four, and a longer outage one year. The four-year average should be reflected in cost of power calculations rather than

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the expected planned outage during the test year for a rate case. If, over time, the actual length of planned outages varies over a five- or six-year cycle, then that should be reflected in rate making.

## THERMAL PLANTS

In the following pages I shall discuss each thermal plant separately. All the data shown are calculated from data now available to me. In the coming weeks I expect Portland General Electric to provide up-to-date data for Boardman. Both Pacific Power & Light and PGE are trying to get Montana Power Company to develop and provide appropriate data for Colstrip.

The data shown below will be changed over time as more recent data is provided by the utilities. For each rate filing the utilities will need to provide updated data and, if necessary, supporting workpapers.

## Portland General Electric

### Trojan

MDC
EOR
Planned Maintenance
Available (Month-to-Month)

1080 mw 16.4% (6/80-5/84) 71 days 609 mw (PGE share) 23 mw (PP&L share) PGE

Primary Utility

The EOR calculated for Trojan is for 48 months calendar June 1980-May 1984. The procedure I used was based on net mwh produced, which reflects all station use mwh and forced outages. The data comes from Trojan's monthly operating data report, which PGE prepares for the NRC and provides a copy to us. I did not calculate EOR on a month-by-month basis. I do exclude economy, planned refueling, and NRC imposed outages.

The underlying rationale for the procedure that I used is that Trojan normally is run at 100 percent of its capability. The evidence I have seen over the years points to that. There have been some clear-cut economy shutdowns, and one partial backdown for a few days for economy reasons in 1984.

The Trojan monthly operating reports show net mwh produced. The narrative part of each report discusses all outages in detail. From the narrative I determine the net hours each month Trojan should have been available by excluding refueling hours, NRC imposed shutdown hours, economy, and equivalent economy shutdown hours. I sum the net hours available and the net mwh produced over 48 months. The average mw available from Trojan is the sum of mwh divided by the sum of net hours.

For Trojan, I think the annual planned refueling and maintenance outage will vary from 61 to 80 days. The average is about 71 days. Trojan had two very long refueling outages in 1982 and 1983, which

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would tend to lengthen the average refueling outage. The 1982 refueling outage includes a 1-month forced outage (leaking pressurizer) which is reflected in my calculations for EOR. However, both the 1982 and 1983 refueling outages were effectively extended because of good hydro conditions and both, therefore, are partially economy shutdowns. Those long refueling outages were adjusted before the average refueling outage duration was realculated. Therefore, I believe the average refueling outage for Trojan should be about 71 days. I developed that number in detail for my testimony in the 1983 Portland General Electric rate case, UE 1/UE 6. The average refueling outage, as adjusted, for four years, 1980 through 1983, is 71 days.

In PGE's 1983 general rate case staff settled with the company, for that case only, on a complicated method to account for Trojan's performance to be used in cost of power calculations. The company made four computer runs, for four repetitions of the test year, changing Trojan's available mw each month to show actual mw produced each month over the past four years. That method is not satisfactory. It is complicated, it entails a lot of hand calculations to average four years' results, and it does not theoretically represent Trojan's expected output over a test year. It does not account for variations in other resources. We are treating one resource, that is Trojan, philosophically different from all the other resources.

I propose we use the most recent 48 months of Trojan's historical performance to estimate available megawatts, the same as for other thermal plants. In general, regulatory (NRC) shutdowns should be excluded because they are extraordinary events. Like other thermal plants, planned maintenance and economic outages are also excluded from the calculation of megawatts available. Of course, the planned refueling outage must be represented in annual power cost calculations on an expected average basis.

Only one computer run of PGE's Power Operations Model, which is the new power cost model, is to be used to calculate the cost of power. The procedure of making four computer runs to cover four years of data is not a theoretically sound way to predict next year's cost of power, nor Trojan's performance. There are some additional power costs which result when the old power cost model is run four times using actual mw for Trojan versus one computer run using average mw for Trojan. Those additional calculated power costs will be reduced in the future because Colstrip #3 is now on line. Colstrip #3 is a low operating cost unit. Its existance will reduce variations in power cost resulting from variations in Trojan's mw\_output.

In PGE's 1983 general rate case, UE 1/UE 6, the difference in cost of power between four computer runs and one equivalent run was about \$765,000. The one run produced the lower cost. After considering PGE's power cost adjustment, the cost to PGE is about \$153,000. PGE's total cost of power is about \$127,000,000. The

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cost to PGE from using one computer run is about 0.012 percent of their total power cost. Power cost predictions are never anywhere near that accurate, so using one computer run instead of four is well within normal accuracy limits.

I have shown an Equivalent Outage Rate (EOR) for Trojan of 26.4 percent. That translates into using 609 mw available at Trojan for PGE. Actually the 16.4 percent EOR is fiction. It reflects thousands of megawatt hours of non-running station use; however, the 609 mw itself is reasonable. PGE's power operations model includes a non-running station service as a separate line item. That line item includes non-running station service for Trojan and for Boardman. Because I exclude station service from available mw, that separate line item must be eliminated.

For Trojan, I suggest we use the average of actual historical mw produced at Trojan over the most recent rolling 48 calendar months. We will not calculate EOR as such, nor availability as a percentage. Of course, we will exclude regulatory, planned refueling, and the economy shutdowns, both full and partial, from the 48-month average.

### Boardman

MDC EOR Planned Maintenance Available 530 mw
14.2%
4 weeks
356 mw (PGE share)
44 mw (IPC share)
PGE

Primary Utility

The available mw excludes station use. The EOR shown is calculated from 38 months, August 1980 through September 1983 of actual, 13.7 percent, and 10 months of national average, 16.2 percent forced outage rate. The national average data is shown on page 3 of the appendix attached to this memo. For coal plants of Boardman's size for the fourth year of operation, the average forced outage rate is 16.2 percent. In PGE's next general rate filing there will be 48 months of actual data available from Boardman, so the national average data will not be used.

The Equivalent Outage Rate that I have calculated for Boardman excludes all outages caused by the turbine blade problem. Also, it excludes planned and economy shutdowns. There are two reasons for excluding the turbine blade outages. One reason is that the problem was extraordinary. The Oregon PUC, as well as all jurisdictions, does not consider extraordinary, nonrecurring events for rate making. We set rates based on normal, ongoing expected conditions.

The second reason is that the turbine blade problem has been repaired. It was repaired in the spring of 1982. There was an additional fix made to the turbine blades in September 1983.

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## Colstrip #3

MDC
EOR
Planned Maintenance
Available
Primary Utility

700 mw
17.3%
4 weeks
116 mw (PGE share)
58 mw (PP&L share)
PGE & PP&L

The EOR shown is for the first year only. It was taken from the national average data for the first year of service, which are shown on page 3 of the appendix. For the second year of operation we will calculate a weighted EOR using several months' actual data as available, and subsequent years national average forced outage rates. In addition, we will assess an appropriate planned maintenance duration, for the second and future years of operation.

### Colstrip #4

MDC EOR Planned Maintenance Available

Primary Utility

700 mw
17.3%
4 weeks
116 mw (PGE share)
58 mw (PP&L share)
PGE & PP&L

The EOR shown is for the first year only. It is taken from the national average data for the first year of service, which are shown on page 3 of the appendix.

## Idaho Power Company

## Valmy 1

MDC EOR Planned Maintenance Available Primary Utility 264 mw 6.96% 4 weeks

115 mw (IPC share)

The EOR shown is calculated from 29 months, late December 1981 through May 1984, of actual data at 6.4 percent, seven months of third year national average data at 7.7 percent, and five months of fourth year national average data at 9.2 percent.

The actual data was taken from a Unit Data Summary report through May 1984, supplied by Idaho Power Company.

## Valmy 2

MDC EOR Planned Maintenance Available Primary Utility 264 mw
12.8%
4 weeks
115 mw (IPC share)
IPC

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> The EOR shown is taken from the national average, for the first year of operation, for coal plants of Valmy's size.

## Pacific Power & Light

The following data for four Pacific Power & Light plants is calculated from the monthly unit data summary for each unit for April 1984. The data reflects 48 months of operation for each unit through April 30, 1984. The planned maintenance shows Pacific Power's long-term cycle average for planned outage duration for each plant. The days outage duration shown are unit-days.

19.6%

PP&L

345 mw

1529 mw

## Jim Bridger 1-4

MDC EOR Planned Maintenance Available.

Primary Utility

## Dave Johnston 1-4

MDC EOR Planned Maintenance Available Primary Utility

## Wyodak

MDC EOR Planned Maintenance Available Primary Utility

785 mw (total 4 units) 13.0% 113 days (total) 633 mw ( " ) PP&L

510 mw each (2040 mw total)

1019 mw (PP&L share, total) 510 mw (IPC share, total)

148 days (total 4 units)

# 3.5% . 28 days

241 mw (PP&L share) PP&L

## Centralia. 1-2

MDC EOR Planned Maintenance Available Primary Utility

665 mw each (1330 mw total) 13.1% 74 days (total 2 units) 522 mw (PP&L share, total) 27 mw (PGE share, total) PP&L

The above data for each MDC rating reflects the data available to me now. For each rate filing the utilities will need to provide up-to-date information and, if necessary, supporting documents.

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# PLANNED AND ECONOMY OUTAGES

The EOR indicated for the above thermal plants was calculated excluding planned and economy outages. Where data was available, the EOR was calculated as a 48-calendar month average. For rate making, cost of power calculations will use (1.0 - EOR) \* (MW Net) as the unit or plant megawatts available for the several months each year the unit is scheduled to be on line. In addition, the cost of power calculations need to reflect planned maintenance outages for each unit or plant.

For the coal plants listed earlier, annual planned maintenance varies from three to six weeks. I prefer that utilities use a long-run cycle average for planned outage duration for rate making. As an alternative, the above estimates of annual planned maintenance may be altered annually by the utilities with staff's concurrence to reflect the expected maintenance schedule for the test period used in a rate case.

The procedure I propose excludes reserve shutdown (economy outages) and planned maintenance outages from the calculation of Equivalent Outage Rate (EOR). Economy and planned outages do not count for nor against utilities. If we use this procedure, then the theoretical problem of considering a unit as 100 percent available during a reserve shutdown does not exist. PGE and PP&L have argued that a plant should not be considered 100 percent available when it is not running, because if it were operated there would be, on average, some forced outages. Their's is a reasonable argument.

Occasionally we will need to determine if an outage was a forced or a reserve (economy) shutdown. The outage will be considered a reserve (economy) shutdown unless the utility provides a clear, definite explanation of the cause.

# GENERAL INFORMATION

The only thermal plants of concern in this memo are those discussed earlier. Some data about each plant is also listed in the attached appendix. Beaver and other combustion turbines and diesel units are not covered by this memo because their maximum performance, or maximum available mw, have not been serious issues in rate making.

I do not suggest the PUC accept "carte blanche" whatever Equivalent Outage Rate (EOR) or MW Net the utilities calculate for each unit, even if such actually occurred. As in all aspects of rate making, if we can reasonably establish that substandard performance was due to poor or imprudent management then we can and should disallow some cost or adjust the historical EOR or MW Net. That applies even to data I have shown earlier.

The list of thermal plants discussed earlier and also shown in the appendix indicates the primary utility, i.e., Portland General Electric, Idaho Power Company, or Pacific Power & Light. The primary utility is the one the PUC staff generally will expect to furnish data

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for the unit and to estimate planned maintenance outages. However, if the primary utility does not furnish appropriate data, the other involved utilities will not be excused.

An exception is Colstrip. There, for the time being, I propose to treat PGE and PP&L as each being responsible to develop the relevent data; however, they need not act independently. I suggest that each act as a check on each other and on Montana Power.

Usually the procedures, data, and results we settle on for the primary utility will be applied to the other utilities for each plant. I am sure there will be exceptions over the years.

bjs/1710m

Attachments

Appendix A Pg. 1

## Thermal Plant Performance

Plant	48 Months EOR <sup>1</sup>	48 Months Thru
Trojan	16.4%	5/84
Boardman	14.2	9/83²
Colstrip 3	17.3 <sup>3</sup>	As of on-line date (1/10/84)
Colstrip 4	17.3	As of on-line date
Valmy 1	7.9	7/83²
Valmy 2	12.8	As of on-line date
Bridger 1-4	19.6	4/84
D. Johnston	13.0	n'
Wyodak	3.5	n n
Centralia 1-2	13.1	<b>u</b>

<sup>&#</sup>x27;EOR in percent

<sup>&</sup>lt;sup>2</sup>EOR includes actual and additional one year from national averages.

<sup>&#</sup>x27;National average data. For illustration only until actual performance data is available.

Appendix A Pg. 2

Thermal Plants

Plant	` MDC mw¹	Primary Utility <sup>2</sup>	Percent Share	Other Utility	Percent Share
Trojan	1080 mw	PGE	67.5%	PP&L	2.5%
Boardman	530	PGE	80.0	IPC	10.0
Colstrip 3	700	PGE	20.0	PP&L3	10.0
Colstrip 4	700	PGE	20.0	PP&L3	10.0
Valmy 1	254	IPC	50.0	•	
Valmy 2	254	IPC	50.0		
Bridger 1-4	510 each	PP&L	66.7	IPC	33.3
D Johnston	785 total	PP&L	100.0		
Wyodak	345	PP&L	80.0		
Centralia 1-2	665 each	PP&L	47.5	PGE	2.5

<sup>&</sup>lt;sup>1</sup>Nameplate rating.

<sup>&</sup>lt;sup>2</sup>Primary utility for providing data and planned maintenance schedules for Oregon rate making.

For Colstrip PP&L will also be treated as the primary utility.

Appendix A Pg. 3

## Thermal Plants

First four years of service. Values to be averaged with actual performance for plants less than four years old.

Plant	Nameplate MW	. 1st FOR <sup>2</sup>	Tear of S  2nd  FOR	ervice¹ 3rd FOR	4th FOR
Boardman <sup>3</sup>	530				16.2
Colstrip 3 & 4	700 ea	17.3	14.7	12.3	15.7
Valmy 1 & 2	254 ea	12.8	6.4	7.7	9.2

Data: FOR in percent. National figures.

Source: PNUCC Thermal Resources Data Base
Addendum February 1, 1983.

PNUCC source is North American Electric Reliability Council (NERC).

<sup>2</sup>EOR, Forced Outage Rate

'It is expected 48 months data for Boardman will be available before PGE's next rate filing.

jcp/1014j-3

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 103** 

**Exhibits in Support of Opening Testimony** 

## PacifiCorp Coal Fired Units 2005-2008 Staff Data Request #5

49.7	Data	
Unit ID	Sum of Non-Forced hours during Low Load Period*	Sum of Non-Forced hours during High Load Period*
CHO-4	54	37
COL-3	270	224
COL-4	304	227
CRB-1	494	265
CRB-2	772	527
CRG-1	0	. 0
CRG-2	42	19
DJ-1	25	40
DJ-2	60	59
DJ-3	22	5
DJ-4	211	231
HDN-1	179	266
HDN-2	171	236
HTG-1	1,419	1,332
HTG-2	1,039	787
HTR-1	1,179	1,146
HTR-2	1,653	1,500
HTR-3	1,448	1,361
JB-1	553	443
JB-2	471	194
JB-3	571	275
JB-4	412	290
NTN-1	1,464	708
NTN-2	1,692	814
NTN-3	1,439	933
WYO-1	515	476
<b>Grand Total</b>	16,458	12,396

**Total Hours for all Coal plants** 

28,854

% Low Load Hours % High Low Hours 57% 43%

<sup>\*</sup>Non forced activity is defined as: Maint. Outages, maint. Extensions, planned derates, & maint. Derates.

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 104** 

**Exhibits in Support of Opening Testimony** 

1,413 MW	MW	Plant Capacity														
The state of the s	Grand Total	Forecast	Naïve	Forecast 2 )	year	Forecast 3	3 year	Forecast 4								
Jim Bridger	Hours	Naïve	% error	2 year rolling avg %	error	3 year rolling avg. %	% error	4 year rolling avg %	% error 5	5 year rolling avg %	% error	6 year rolling avg % e	% error 4 ye	4 year weighted avg	% error weights	eignts
1979	3,535,641															0.0
1980	3,803,416															0.20
1981	4,193,370		-16%													S 6
1982			87%	3,669,529	%08											04.0
1983	1,708,626		145%	3,998,393	134%	3,844,142	125%									
1984	1,194,910	2,035,950	%02	3,114,660	161%	3,344,245	180%	3,392,094	184%				<del></del>	3,186,638	16/%	
1985	_	1,708,626	16%	1,872,288	27%	2,645,982	%62	2,935,340	%66	3,055,401	107%			2,513,251	%0/	
1986		_	33%	1,451,768	62%	1,646,495	84%	2,283,214	155%	2,587,254	189%	_	207%	1,817,079	103%	
1987	_	_	2%	1,335,307	%8-	1,459,747	1%	1,603,797	11%	2,121,712	47%	2,401,996	%99	1,494,075	%	
1988			-38%	_	-18%	1,188,604	-18%	1,318,609	%6-	1,462,077	1%	1,917,293	35%	1,210,635	-12%	
1989	_	_	%6-	_	-26%	1,272,286	-50%	1,252,942	-21%	1,344,079	-15%	1,459,391	-8%	1,261,574	-21%	
1990		_	42%		45%	1.264.059	24%	1,316,970	78%	1,292,558	27%	1,361,903	34%	1,340,806	32%	
1991	_	_	-5%	_	-7%	1,494,687	-8%	1,344,814	-17%	1,370,992	-16%	1,341,645	-17%	1,448,850	-11%	
1997	_	_	-10%		15%	1.352.137	20%	1,375,592	25%	1,279,513	13%	1,312,212	16%	1,318,248	17%	
1993			8%		-15%	1,410,459	%9-	1,420,599	-2%	1,425,671	-2%	1,337,259	-11%	1,418,406	<b>%9-</b>	
1994		_	-4%		17%	1,258,150	2%	1,340,383	14%	1,362,511	16%	1,376,418	17%	1,302,228	11%	
1995			31%		15%	1.419,702	24%	1,319,354	15%	1,372,899	50%	1,385,919	21%	1,367,260	19%	
1996		_	-22%		-11%	1.269.821	-16%	1,358,862	-10%	1,290,752	-14%	1,340,140	-11%	1,310,056	-13%	
1997	_		-22%		-21%	1,275,415	-13%	1,239,100	-16%	1,316,477	-10%	1,266,782	-14%	1,225,286	-16%	
1998	_	_	21%	_	%9	1,275,536	5%	1,332,393	%/	1,291,945	<b>4</b> %	1,347,619	8%	1,330,977	%	
1999			-4%	_	-3%	1,372,410	-10%	1,323,394	-14%	1,359,308	-11%	1,321,116	-14%	1,384,807	-10%	
2000	_		5%	_	11%	1,405,934	15%	1,341,184	10%	1,308,216	42	1,340,674	10%	1,354,452	11%	
2001		_	20%	_	%6	1,415,750	11%	1,437,644	13%	1,379,503	8%	1,345,643	2%	1,431,088	15%	
2002		_	-49%	_	-45%	1,333,900	-44%	1,367,167	-45%	1,394,399	-41%	1,353,155	-43%	1,344,598	-43%	
2003		_	-54%	_	-55%	1,343,247	-51%	1,319,312	-52%	1,348,843	-51%	1,374,590	-20%	1,307,950	-52%	
2004			-3%	_	-56%	1,623,771	-34%	1,601,022	-35%	1,530,319	-38%	1,519,760	-38%	1,729,964	-59%	
2005			8%	2.560,554	1%	2,132,218	-16%	1,904,518	-55%	1,830,170	-58%	1,733,059	-35%	2,188,259	-14%	
2006	7		19%		79%	2,523,755	23%	2,211,703	%/	2,013,646	-5%	1,933,501	%9-	2,406,516	17%	
2007			20%		18%	2,577,084	22%	2,526,400	20%	2,276,229	%8	2,100,427	%0	2,535,568	20%	
													100	1001001	1007	
Average	1,607,751	1,825,211	11%	1,778,682	16%	1,725,981	16%	1,661,100	14%	1,609,326	% <b>6</b>	1,573,446	%8	1,634,624	\$	
Maximum Value	2.748.759	2.746.759	42%	2.598.459	62%	2,645,982	84%	2,935,340	155%	3,055,401	189%	2,745,319	207%	2,535,568	103%	
Minimum Value	895,198		-54%	The second second	-55%	1,188,604	-51%	1,239,100	-52%	1,279,513	-51%	1,266,782	~20%	1,210,635	-52%	
Median error		1,502,964	2%	1,384,106	%8	1,410,459	2%	1,363,014	7%	1,372,899	1%	1,368,247	-3%	1,376,034	2%	
		014 710	440/		400/	262 UPA	7063	583 598	7053	480 993	K104	401 219	62%	530.125	47%	

Forecast Trending Analysis

Plant Capacity
| Forecast 2 year Porecast 2 year Forecast 3 year Porecast 4 year Forecast 6 year Forecast 6 year Forecast 8 weights | Forecast 8 year rolling avg % error 2 year rolling avg % error 3 year rolling avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % error 6 year rolling avg % error 7 year weighted avg % erro %9 %89 178% -64% 137,300 81,627 30,240 154,871 130,372 106,685 102,205 86,407 77,708 56,969 56,969 56,801 57,989 57,308 57,30 12% 76% 120,826 49,124 114, 185 1120, 826 113, 728 80, 858 80, 858 77, 841 77, 221 49, 124 49, 124 49, 124 64, 811 90, 288 100, 728 10 81,836 10% 69% 125,591 47,983 82,206 25,540 10% 134,444
132,860
129,336
94,331
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110,993 132,860 83,738 172% -65% 5% 65% 95,715 125,084 125,084 101,375 98,905 94,942 94,942 94,307 55,009 15,009 17,341 120,175 1120,175 1120,217 81,263 81,266 83,446 81,266 8 80,683 -5% 117,861 1103,805 1161,028 1611,028 1114,996 182,723 53,917 54,043 62,754 62,754 62,754 64,559 61,043 92,318 1142,941 1162,941 1162,941 82,355 53,070 136,796 1 161,915 30,706 81,627 35,805 -17% 95% -65% 79,533 156,189 1422 250,634 73,197 74,134 110,611 140,611 29,538 70,418 39,519 71,22 71,237 71,237 72,234 73,237 74,688 109,989 117,64 74,134 175,943 21,893 86,320 19, 533 179, 533 156, 189 151, 422 250, 634 173, 197 110, 611 54, 834 55, 933 55, 933 55, 933 173, 221 61, 731 47, 387 175, 943 137, 649 1 175,943 21,893 80,358 172 MW Grand Total Median error Standard Deviation Minimum Value Carbon

Forecast Trending Analysis

762 MW	762 MW	Plant Capacity	.≱											o <b>o</b>		
	ind Total	Forecast	200	Forecast	100000						347	51600	6 year			
Dave Johnston	Hours	Naive	% error	2 year rolling avg	% error	3 year rolling avg. 7	% error	4 year rolling avg % error	or 5 year rolling avg	-	% error o	o year rolling avg 76	70 error	4 year weignted avg %	% error weignts	0 10
1980							-									0.20
1981		698,264	-50%													0.30
1982	2 660,891	626,376	-2%	662,320	%0											0.40
1983	3 536,000	872,867	63%	749,622	40%	732,503	37%									
1984		660,891	-21%	766,879	%6-	720,045	-14%		-15%					721,318	-14%	
1985		536,000	-28%	598,445	-19%	689,919	-7%	674,033 -	%6-		-8%			649,878	-12%	
1986	343,544	839,288	144%	687,644	100%	678,726	%86	•	12%		%90	705,614	105%	715,980	108%	
1987			117%	790,303	131%	705,536	106%	_	103%	•	114%	712,790	109%	721,603	111%	-
1988			-30%	542,431	10%	641,384	30%	615,038 24	24%	624,208	26%	665,651	35%	581,271	18%	
1989			-43%	342,616	•	475,517	-21%	566,460	%9-	560,368	-1%	577,121	4%	471,931	-25%	
1990			37%	417,960		393,155	%6		33%		23%	549,345	25%	443,040	23%	
1991			61%	549,156	46%	480,000	28%	445,886 19	19%		34%	560,692	49%	492,593	31%	
1992			%6	482,513		486,419	47%		36%		30%	480,968	46%	458,618	39%	
1993			16%	368,608	14%	447,098	38%	458,882 4	41%	435,443	34%	420,127	30%	429,031	35%	
1994			3%	353,260		355,822	11%		30%		35%	417,911	30%	377,578	17%	
1995		324,386	-35%	327,318		343,635	-28%	·	.27%		-17%	415,027	-13%	340,178	-59%	
1996		321,660	-57%	323,023		325,432	-56%	,	-54%	342,702	24%	386,265	-48%	329,657	-26%	
1997			-13%	400,552		375,163	-35%	•	34%		34%	365,493	-34%	386,178	-30%	
1998		741,405	4%	610,424		514,170	-28%	466,724 -3	34%		-38%	428,902	40%	537,166	-24%	
1999	9 813,348	553,959	-35%	647,682	-50%	591,602	-27%	524,117 -3	-36%	484,171	40%	458,517	-44%	572,060	-30%	
2000		710,365	-17%	632,162		929,216	-22%	621,2932	.28%		-35%	521,870	-39%	646,559	-25%	
2001	1 648,287	813,348	25%	761,857		692,557	7%	704,769	%6	659,704	7%	603,363	%/-	723,381	12%	
2002		857,930	76%	835,639		793,881	17%	733,900	9%	735,401	%8	692,742	5%	784,645	16%	
2003		648,287	% <del>9</del> -	753,108		773,188	12%	•	10%	716,778	4%	720,882	2%	750,400	%6	
2004	592,996	678,612	14%	663,449	12%	728,276	23%	749,544	79%	741,708	25%	710,417	20%	718,851	21%	
2005			%89	683,004		671,431	64%		%52	737,114	80%	732,656	%62	693,992	%69	
2006			-13%	640,196	%/-	653,001	-2%	651,823	-2%	693,044	1%	713,095	4%	643,968	%9-	
2007	689'099 2	409,575	-38%	501,286	•	563,322	-15%	592,145 -1	%0	603,373	%6-	645,799	-5%	547,069	-17%	
	000,144		100		7007		7077			400	1007	202 200	7027	010 013	/007	
Average	554,568	5/8,498	8	580,441	%0L	580,014	% L	5/5/614	%11%	9/1,108	\$ 2	116,186	% C	9/2/3	%0L	
Maximum Value	857,930	857,930	144%	835,639	131%	793,881	406%	757,483 11	112%	741,708	114%	732,656	409%	784,645	111%	
Minimum Value	321,660	321,660	-57%	323,023	%95-	325,432	<b>%9</b> 9-	338,1415	-54%	342,702	-54%	365,493	~48%	329,657	<b>%9</b> 9-	
											i		1	a co oma	700	
Median error		604,079	% <b>5</b> -	621,293	10%	641,384	%6	603,591	8%	561,367	84	208,807	8	9/8/88	%0L	
			7007				7007	The distribution of the Control of t		001 101	1027	669 667			ACCOUNT OF THE PARTY OF THE PAR	

precast Trending Analysi

	Grand Total	Forecast	Naïve	Forecast	2 year	Forecast	3 year	Forecast 4	4 year	Forecast 5			233		
Hunter	Hours	Naïve	% error	2 year rolling avg	% error	3 year rolling avg. %	% error 4	4 year rolling avg %	% error	5 year rolling avg %	% error 6	6 year rolling avg %	% error	4 year weighted avg	% error Weights
1979	193,925	15													
1980	377,527														
1981			-54%												
1982		377,527	-35%	285,726	-48%										
1983	1,232,936	3 417,805	%99-	397,666	%89-	329,752	-73%								
1984	559,322	553,434	-1%	485,620	-13%	449,589	-50%	385,673	-31%					441,613	-21%
1985	433,049	1,232,936	185%	893,185	106%	734,725	%02	645,425	46%	555,125	28%			780,518	80%
1986	1,754,306		%89-	896,129	49%	781,897	-55%	690,874	-61%	628,205	-64%	555,825	%89-	746,077	-27%
1987			-32%	496,185	-22%	741,769	16%	694,685	%6	639,309	%0	595,679	-1%	642,947	%
1988	863,099	1,754,306	103%	1,093,677	27%	915,559	%9	994,903	15%	609'906	2%	825,142	4%	1,066,795	24%
1989	<u>-</u>		-36%	1,197,036	20%	942,374	% <del>9</del>	846,611	-15%	923,876	%8 <u>-</u>	862,135	-14%	924,740	% 8-
1990		660,598	13%	751,433	-5%	1,085,724	45%	922,555	20%	849,908	11%	913,746	19%	931,336	22%
1991		<u>-</u>		932,316	20%	834,800	7%	1,064,676	37%	938,351	21%	875,179	13%	962,927	24%
1992			•	883,722	-22%	876,848	-22%	817,578	-28%	1,004,923	-11%	909,611	-19%	843,421	-52%
1993		9 777,519			424	848,321	94%	852,016	%56	995'608	85%	967,022	121%	827,397	86%
1994		<u>-</u>	%69	pace.	45%	890,877	33%	918,541	37%	907,453	36%	862,838	78%	938,271	40%
1995					135%	781,256	134%	777,420	133%	822,242	146%	829,052	148%	745,674	123%
1996				553,052	%9-	745,101	27%	753,206	78%	755,747	78%	796,711	36%	702,328	20%
1997	1,046,044	333,681	%89-	501,368		479,928	-54%	642,246	-39%	669,301	-36%	685,402	-34%	534,518	-49%
1998	933,964	4 585,867	-37%	459,774	-51%	529,534	-43%	506,413	-46%	026'089	-35%	655,395	-30%	511,967	-45%
1999	1,252,890	1,046,044	-17%	815,956	-35%	655,197	-48%	658,662	-47%	614,339	-51%	700,149	-44%	727,819	-45%
2000	1,688,883	3 933,964		990,004	-41%	855,292	-49%	724,889	-21%	713,722	-58%	667,610	%09-	837,940	-20%
2001		0 1,252,890		1,093,427	-27%	1,077,633	-58%	954,691	-63%	830,489	%89-	803,583	<b>%69</b> -	1,049,141	-29%
2002	980,210	1,688,883			20%	1,291,913	32%	1,230,445	79%	1,101,530	12%	973,555	-1%	1,342,818	37%
2003	1,300,685	5 2,562,500	_	2,125,692	93%	1,834,758	41%	1,609,559	24%	1,496,856	15%	1,345,025	3%	1,875,639	44%
2004	1,177,356	980,210	Ċ		20%	1,743,864	48%	1,621,121	38%	1,483,689	76%	1,410,749	20%	1,623,899	38%
2005	1,168,728	1,300,685	11%		-5%	1,614,465	38%	1,633,069	40%	1,557,034	33%	1,453,189	24%	1,495,725	28%
2006	962,304	4 1,177,356	3 22%	1,239,020	78%	1,152,750	20%	1,505,187	26%	1,541,927	%09	1,493,754	22%	1,313,440	36%
2007	961,772	-		1,173,042	22%	1,215,590	79%	1,156,745	70%	1,437,896	20%	1,479,727	24%	1,178,856	23%
Average	1,018,494	4 919,861	7%	929,035	7%	936,381	8%	941,966	40%	948,655	40%	939,140	8%	960,242	11%
Maximum Value	2,562,500	2,562,500	185%	2,125,692	135%	1,834,758	134%	1,633,069	133%	1,557,034	146%	1,493,754	148%	1,875,639	123%
Minimum Value	333,681		-68%	459,774	-57%	479,928	%89-	506,413	-63%	555,125	%89-	555,825	<b>%69</b> -	511,967	%69-
3		000 630	407		/06	000 330	460/	9.40.343	200,	849 908	7061	787 487	70.1	884 084	7066
Median error		000,088		100,400	2.7.	767'660	8 2	010,000	202	000,500	8 100	100,000	2000		7007
The second secon	VACITY DESCRIPTION AND ADDRESS OF THE PARTY.	AND	The second secon				Woodham Charleson	22.5	Contract Con		CONTROL OF THE PARTY OF THE PAR	100 E 100 E	- Continue of the Continue of		

Forecast Trending Analysis

CASE: UM 1355

WITNESS: KELCEY BROWN

# PUBLIC UTILITY COMMISSION OF OREGON

**STAFF EXHIBIT 105** 

**Exhibits in Support of Opening Testimony** 

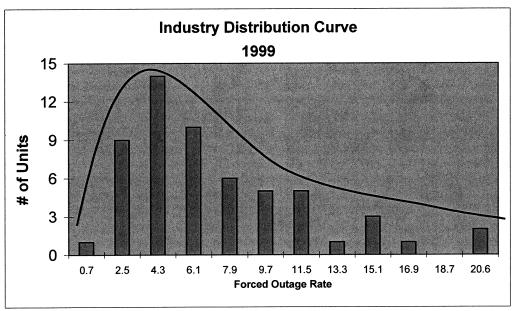
Coal Fossil Units 6 NERC Data	00-699 <b>M</b> W		7.00						
Units	1999	2000	2001	2002	2003	2004	2005	2006	2007
1	0.69	0.91	0.01	0.00	0.42	0.19	0.10	0.22	0.07
2 3	1.06	1.00	0.33	0.09	0.50	0.38	0.46	0.47	0.18
3	1.33	1.62	0.60	0.54	0.63 0.75	0.96 1.01	0.84 0.88	0.60 0.62	0.21 0.24
4	1.81	1.67 1.70	0.88 0.99	0.63 0.64	1.32	1.01	1.14	0.02	0.24
5 6	1.91 1.94	1.77	1.00	0.70	1.35	1.23	1.30	1.27	1.04
7	1.97	2.00	1.14	0.72	1.36	1.42	1.60	1.33	1.22
8	2.42	2.04	1.21	0.79	1.42	1.48	1.69	1.40	1.25
9	2.46	2.10	1.26	0.83	1.54	1.59	1.81	1.64	1.50
10	2.49	2.15	1.40	0.92	1.59	1.67	2.03	1.91	1.95
11	2.57	2.50	1.90	0.94	1.60	1.93	2.07 2.39	1.94 2.03	2.00 2.05
12	2.77	2.53	1.92 2.04	0.98 1.12	1.70 1.78	1.97 2.06	2.39	2.03	2.03
13	2.92 2.99	2.54 2.60	2.04	1.12	1.70	2.26	2.51	2.41	2.41
15	3.11	2.68	2.19	1.30	1.83	2.40	2.62	2.58	2.61
16	3.12	2.81	2.37	1.37	1.91	2.57	2.85	2.94	2.99
17	3.22	3.03	2.56	1.42	2.08	2.58	2.94	2.98	3.29
18	3.25	3.06	3.25	1.55	2.29	2.70	3.00	3.06	3.40
19	3.47	4.18	3.35	1.59	2.53	2.97	3.05	3.24	3.46
20	3.71	4.22	3.84	1.64	2.75 3.18	3.14 3.34	3.38 3.63	3.33 3.48	3.75 3.79
21	3.89 4.01	4.34 4.51	3.93 4.33	1.72 1.86	3.18 3.35	3.34	4.03	3.46 3.87	3.79
22 23	4.01	4.80	4.50 4.50	1.89	3.91	3.45	4.12	4.20	4.21
24	4.26	4.89	4.60	1.99	3.97	3.67	4.33	4.40	4.71
25	4.37	5.00	4.62	2.70	4.42	3.71	4.34	4.47	5.04
26	4.56	5.05	4.68	2.79	4.50	3.80	4.88	4.62	5.11
27	4.95	5.14	4.78	2.99	5.02	3.84	4.90	4.65	5.21
28	4.98	5.32	4.90	3.10		4.06	5.11	4.71 4.97	5.45 5.52
29	5.23	5.67	5.12 5.47	3.17 3.41	5.30 5.52	4.59 4.67	5.12 5.25	5.15	1 1
30 31	5.33 5.56	5.68 6.02	5.47 5.58	3.50	5.83		5.42	5.26	
32	5.78	6.14	5.87	3.77	5.87		5.45		
33	5.94	6.23	5.98	3.84	5.89	5.07	5.73	5.60	5.80
34	5.95	6.29	6.18	4.17	6.02		5.82	5.92	6.21
35	6.37	6.37	6.90	4.42	6.05		5.95	5.93	
36	6.82	6.69	7.31	4.44	6.07		5.96	6.30	
37	7.10	7.00	7.44	4.52	6.49 6.78		6.50 6.62	6.50 6.52	
38	7.36 7.54	7.10 7.11	7.62 7.69	4.61 4.76	7.03		6.64		
40	7.86	7.11	7.83	4.90	7.18		7.24	1	8.62
41	8.46	7.40	8	5.51		1			
42	8.48	8.68	7.90	5.63			7.66		
43	8.92	8.97	7.91	5.68			7.73		9.53
44	9.08	9.31	8.04	6.07	8.12				
45	9.57	9.97	8.70 9.57	6.73 7.37	8.78 9.37		8.00 8.34	10.26	
46 47	10.17 10.57	10.39 10.86	9.57 10.68	8.02					
48	10.57	11.20	11.51	8.35			9.64		
49	11.17	11.66	12.03	9.42	11.23		10.40	12.36	10.77
50	11.51	12.13	14.02	10.51	13.15	10.42	10.60	12.45	
51	13.17	14.05		10.71	13.92				
52	13.78	14.38		17.06					
53	13.97	14.48		17.74	22.11 23.34				
54 55	14.22 16.71	17.86 23.00		34.51	∠3.34	13.55		24.93	
56	19.24	36.55				14.93			23.25
57	20.55	30.00				16.37			23.85
58	_3.00					30.94			
							40.7-	40.44	40.67
90th percentile	13.41 1.96	13.09 1.89		9.10 0.71					12.67 1.15
10th percentile	1,96	1.69	1.00	0.71	1.00	1.30	1.03	1.23	,,,,,
4 year average 90t	h percenti	le	450 E	11.29				11.47	
4 year average 10t	h percenti	le	200 B	1.39	1.24	1.11	1.20	1.35	1.30

Coal Fossil Units NERC Data	500-599 <b>M</b> V	V							
Units	1999	2000	2001	2002	2003	2004	2005	2006	2007
1	0.18	0.00	0.04	0.00	0.47	0.34	0.60	0.33	0.15
2	0.50	0.13	0.13		0.53		0.71	0.35	
2 3	0.55	0.28	0.19		0.67	0.48	1.36		0.74
4	0.62	0.77	0.36	0.65	0.92		1.54		
5	0.75	1.20	0.37	0.78	1.31		1.58		
6	0.80		0.38	0.87	1.40		1.59		
7	0.81	1.48	0.49				1.75		
8	0.83	1.51	0.63				1.91		
9	1.00	1.59	0.65				1.95		
10	1.06	1.62	0.67						
11	1.16	1.69	0.81 0.91	1.05 1.07					
12	1.20 1.27	1.70 1.82	0.91				2.13		
13 14	1.27	1.02	1.16				2.62		
15	1.38		1.10				2.69		
16	1.72	2.02	1.30				2.71		
17	1.72	2.10	1.33						
18	2.03	2.43	1.34					I .	
19	2.65	2.54	1.40					1	
20	2.66	2.55	1.44	1.94				I .	
21	2.83	2.63	1.49	2.01			3.29		3.22
22	2.89	2.65	1.71	2.13			3.66		3.28
23	3.01	2.74	1.74			2.90	3.83	2.64	
24	3.05	2.76	1.83			2.93			
25	3.25	2.85	1.84						
26	3.39	2.94	1.91						
27	3.52	3.11							
28	3.58								
29	3.64								
30	3.86		2.06						
31	4.01		2.11						
32	4.44							1	
33	4.47	3.63							I .
34	4.54	3.71	2.34						
35	4.66			1	1		l .	I	
36 37	4.83 4.89								
38	4.09	1							
39	5.08								
40	5.27		2.76						
41	5.29								
42	5.41		2.84						
43	5.44					4.46	6.27	4.17	5.31
44	5.51					4.70	6.32		
45	5.58			3.46	5.04				
46	5.61	5.00	3.20	3.57					
47	5.71	5.02							
48	5.77								
49	6.08								
50	6.13								
51	6.16								
52	6.25								
53	6.56								
54	6.87								
55	6.88	5.60	3.89	4.71	6.46	5.95	9.58	5.97	7.99

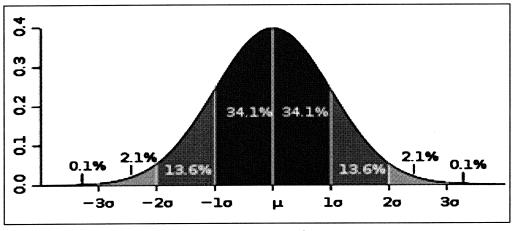
1.54 P. 18	1999	2000	2001	2002	2003	2004	2005	2006	100
56	7.20	5.63	4.11	4.77	7.14	6.08	10.09	5.99	
57	7.25	5.67	4.28	4.78	7.59	6.14	10.14	6.09	
58	7.44	5.76	4.75	4.81	7.70	6.20	10.19	6.78	
59	7.55	5.83	4.97	4.83	7.75	6.33	10.33	6.97	
60	7.66	5.86	5.13	4.94	7.78	6.53	10.37	7.06	
61	7.69	5.98	5.23	5.27	7.95	6.64	10.53	7.27	
62	7.79	6.09	5.29	5.28	7.97	6.70	10.85	7.50	
63	7.86	6.22	5.35	5.46	8.04	6.71	10.94	7.54	
64	8.14	6.30	5.47	5.72	8.06	6.73	11.17	7.59	
65	8.22	6.40	5.54	6.23	8.11	6.85	11.54	7.69	l
66	8.28	6.56	5.56	6.35	8.40	7.14	11.55	7.74	l
67	8.61	6.62	5.76	6.36	9.39	7.55	12.21	7.75	
68	8.62	6.85	6.07	6.39	9.44	7.88	12.29	8.30	
69	8.64	7.18	6.41	6.40	9.49	8.23	12.39	8.44	
70	8.65	7.19	6.55	6.50	9.70	8.26	12.82	8.45	
71	8.73	7.28	6.62	6.72	9.89	8.52	13.25	9.65	
72	8.78	7.36	6.69	6.77	10.47	8.54	13.56	9.97	
73	9.05	7.52	6.71	6.99	10.66	8.72	13.80	10.48	
74	9.18	7.65	7.11	7.03	10.71	8.77	15.62	10.51	
75	9.33	7.66	7.32	7.07	11.10	8.99	15.72	10.61	
76	9.60	7.71	7.40	7.17	11.27	9.02	16.01	11.08	
77	9.85	7.87	7.42	7.31	11.44	9.19	16.18		
78	9.95	7.92	7.89	7.64	11.55	9.37	17.18		
76 79	10.09	8.03	8.02	7.85		9.48	22.68		
80	10.03	8.24	8.07	7.93		9.50	22.99		ı
81	10.14	8.38	8.20	8.11	13.10	9.68	23.02	11.98	
	10.27	8.59	8.47	8.18	13.15	9.78	24.55	1	1
82		9.05	8.63	8.32	13.56	10.26	26.09	i e	
83	10.43		8.70	8.96	15.79	11.20	33.51	i	l
84	10.88	9.37		9.42	16.58	12.02	33.31	12.74	
85	10.90	9.53	10.68	9.42	16.80	12.02		12.74	
86	11.23	9.89	11.17		17.70	12.40		14.62	
87	11.31	9.91	11.59	9.76		13.21		15.96	
88	11.92	10.22	12.66	10.62	18.03	14.15		22.24	l
89	12.33	10.25	12.93	10.98	18.94			23.02	
90	12.38	10.32						23.47	
91	13.26	10.38	14.00					26.41	
92	13.45	11.88	16.31	11.69				20.41	
93	14.03	11.92	16.69						İ
94	14.44	12.09	16.83			16.48		1	
95	14.78	12.66	16.94			17.86			
96	15.27	13.65	21.30		1	20.45			
97	16.80	13.81	21.36			22.61			
98	20.00	19.32	56.15			33.07			
99	24.49	21.34		37.22		39.30			
100	24.92								
101	25.86								
102	89.14								
ercentile	13.431	10.264	12.741	11.056	15.344	14.196	15.923	12.315	
ercentile	1.164	1.676					1.965		*
average 90				11.87	12.35	13.33	14.13	14.44	

1 0.37 0.36 0.00 0.03 1.29 0.54 0.15 0.00 0.8   3 1.54 1.10 0.22 1.27 2.38 0.71 1.02 0.10   4 2.02 1.23 0.48 1.30 2.74 0.94 1.46 0.25   5 2.21 1.58 1.16 1.33 2.95 1.24 1.50 0.34   6 2.33 1.66 1.39 1.40 2.99 1.47 1.78 0.79   7 2.56 1.88 1.45 1.51 3.13 1.93 2.07 1.04   8 2.75 2.26 1.59 1.64 3.18 2.43 2.34 1.17   9 3.09 2.39 1.86 1.66 3.33 2.45 2.65 1.78   110 3.14 2.56 1.88 1.75 3.38 2.61 2.84 2.01   11 3.22 2.67 1.89 1.82 3.46 2.85 2.96 2.22   12 3.28 2.94 1.95 1.94 3.70 2.95 3.27 2.67   13 3.83 3.32 3.14 2.11 3.78 3.03 3.28 2.86   14 3.95 3.60 3.35 2.12 3.90 3.05 3.34 3.11   15 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.19   16 4.42 3.80 3.66 2.59 3.99 3.36 4.53 3.86   17 4.61 3.87 3.73 2.70 4.06 3.41 4.59 4.91   18 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13   18 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13   18 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13   18 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13   19 6.66 4.92 4.07 3.01 4.79 3.47 5.06 5.20   20 7.00 5.21 4.21 3.02 5.09 3.48 5.74 5.56   22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95   23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 5.97   24 7.24 6.37 5.26 3.56 5.98 3.73 6.52 6.39   25 7.26 6.40 5.26 4.01 6.02 3.84 6.72 6.89   27 8.13 7.19 5.67 5.09 6.83 7.75 6.89   27 8.13 7.19 5.67 5.09 6.83 7.76 6.99 5.95   31 1.14 1.19 9.98 8.05 7.71 7.06 8.25 6.89 3.73 6.52 6.39   32 1.14 1.19 9.98 8.05 7.71 7.06 8.25 6.19 9.78 7.79 8.25   33 1.66 9.29 8.01 7.82 9.94 1.99 1.09 1.09 8.20 1.88 8.79   34 1.55 1.55 1.14 1.19 9.01 7.13   38 1.54 8.28 1.19 9 1.03 1.28 5 11.04 9.99 1.76 3.11 1.50 1.55 1 1.15 1.15 1.15 1.15 1.15	RC Data	1999	2000	2001	2002	2003	2004	2005	2006	200
1 1.54			0.36	0.00						0.3
3   1.54   1.10   0.22   1.27   2.38   0.71   1.02   0.10   4   2.02   1.23   0.48   1.30   2.74   0.94   1.46   0.25   5   2.21   1.58   1.16   1.38   2.95   1.24   1.50   0.34   6   2.33   1.66   1.39   1.40   2.99   1.47   1.78   0.79   7   2.56   1.88   1.45   1.51   3.13   1.93   2.07   1.04   8   2.75   2.26   1.59   1.64   3.18   2.43   2.34   1.17   9   3.09   2.39   1.86   1.66   3.33   2.45   2.65   1.78   10   3.14   2.56   1.88   1.75   3.38   2.61   2.84   2.01   11   3.22   2.67   1.89   1.82   3.46   2.85   2.96   2.22   12   3.28   2.94   1.95   1.94   3.70   2.95   3.27   2.67   13   3.83   3.32   3.14   2.11   3.78   3.03   3.28   2.81   14   3.95   3.60   3.35   2.12   3.90   3.05   3.34   3.11   15   4.17   3.69   3.38   2.34   3.97   3.08   4.53   3.86   17   4.61   3.87   3.73   2.70   4.06   3.41   4.59   4.91   18   6.44   4.74   3.77   2.88   4.65   3.43   4.59   4.91   19   6.66   4.92   4.07   3.01   4.79   3.47   5.08   5.20   20   7.00   5.21   4.21   3.02   5.09   3.48   5.74   5.56   21   7.05   5.85   4.84   3.31   5.22   3.67   6.09   5.95   22   7.05   5.85   4.84   3.31   5.22   3.67   6.09   5.95   23   7.17   6.07   5.13   3.46   5.63   3.77   6.27   5.97   24   7.24   6.37   5.25   3.56   5.98   3.73   6.52   6.39   25   7.26   6.40   5.26   4.01   6.02   3.84   6.72   6.46   26   7.48   6.62   5.55   4.15   6.24   3.94   6.97   6.69   27   8.13   7.19   5.67   5.09   6.43   4.05   8.47   7.03   28   8.29   7.31   6.36   6.21   6.51   4.11   9.01   7.13   29   8.45   7.31   7.41   7.69   6.85   6.73   4.90   9.30   7.63   31   9.98   8.05   7.71   7.06   8.25   6.19   9.78   7.95   32   10.12   8.14   7.75   7.75   9.35   6.17   9.92   7.95   33   10.60   9.29   8.01   7.62   9.41   6.94   11.01   8.25   34   10.79   9.37   8.05   8.33   11.49   11.92   1.36   11.55   11.21   8.53   8.99   11.04   9.01   15.48   8.79   34   10.79   9.37   3.65   21.45   11.95   11.55   11.56   11.21   11.55   11.99   11.92   13.76   11.55   11.55   11.99   11.92   13.76   11.55   11.55   11	2									0.5
5 2.21 1.58 1.16 1.38 2.95 1.24 1.50 0.34 6.6 2.33 1.66 1.39 1.40 2.99 1.47 1.78 0.79 1.04 1.87 2.56 1.88 1.45 1.51 3.13 1.93 2.07 1.04 1.87 2.99 3.09 2.39 1.86 1.66 3.33 2.45 2.45 2.65 1.78 1.00 3.14 2.56 1.88 1.75 3.88 2.61 2.84 2.01 1.1 3.22 2.67 1.89 1.62 3.46 2.85 2.96 2.22 1.2 3.28 2.94 1.95 1.94 3.70 2.95 3.27 2.67 1.3 3.83 3.32 3.14 2.11 3.76 2.95 3.27 2.67 1.3 3.83 3.32 3.14 2.11 3.78 3.03 3.28 2.86 1.4 3.95 3.60 3.55 2.12 3.90 3.05 3.34 3.11 1.5 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.19 6.66 4.42 3.80 3.65 2.59 3.99 3.36 4.53 3.88 1.7 6.60 3.37 2.70 4.06 3.41 4.59 3.86 1.7 6.66 4.92 4.07 3.01 4.79 3.47 5.08 5.20 2.07 7.00 5.21 4.21 3.02 5.09 3.48 5.74 5.56 2.21 7.01 5.66 4.70 3.26 5.18 3.54 6.00 5.89 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 5.97 2.24 7.24 6.37 5.25 3.56 5.95 4.15 6.24 3.94 6.97 6.69 5.95 2.25 7.26 6.40 5.26 4.01 6.02 3.84 6.72 5.97 6.69 5.95 2.27 7.85 8.82 7.31 6.36 6.21 6.61 4.11 9.01 7.13 2.99 8.45 7.35 7.52 6.35 6.69 4.54 9.92 7.72 2.99 8.45 7.35 7.52 6.35 6.69 4.54 9.92 7.72 7.22 8.84 7.73 7.79 5.67 5.99 6.43 4.05 8.47 7.03 3.1 9.98 8.05 7.71 7.06 8.65 6.73 4.90 9.30 7.63 3.1 0.60 9.29 8.01 7.82 9.80 7.71 7.06 8.25 6.19 9.78 7.69 9.30 7.63 3.1 0.60 9.29 8.01 7.82 9.35 6.71 9.99 9.37 8.05 8.33 10.42 7.74 12.26 8.56 1.99 9.37 13.32 12.26 10.99 9.67 12.14 9.99 1.15 1.50 1.15 1.15 1.15 1.15 1.15 1.15	3									0.
6 2.33 1.66 1.39 1.40 2.99 1.47 1.78 0.79 7 2.56 1.88 1.45 1.51 3.13 1.93 2.24 1.17 1.99 3.09 2.39 1.86 1.66 3.38 2.45 2.65 1.78 1.00 3.14 2.56 1.88 1.75 3.83 2.46 2.85 2.96 2.22 1.2 3.26 2.67 1.89 1.82 3.46 2.85 2.96 2.22 1.2 3.28 2.94 1.95 1.84 3.70 2.95 3.27 2.67 1.33 3.83 3.32 2.45 2.96 2.22 1.2 3.26 2.94 1.95 1.94 3.70 2.95 3.27 2.67 1.33 3.83 3.32 3.44 2.11 3.78 3.03 3.28 2.26 1.4 3.95 3.60 3.35 2.12 3.90 3.05 3.34 3.11 1.5 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.19 1.6 4.42 3.80 3.65 2.59 3.99 3.36 4.53 3.86 1.7 4.61 3.87 3.73 2.70 4.06 3.41 4.59 4.91 1.8 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13 1.9 6.66 4.92 4.07 3.01 4.79 3.47 5.08 5.20 2.07 7.00 5.21 4.21 3.02 5.09 3.48 5.74 5.56 2.27 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.22 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 6.09 5.95 2.23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 6.09 5.95 2.23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 6.09 5.95 3.26 6.24 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1										1.
7										2.
8 2.75 2.26 1.59 1.64 3.18 2.43 2.34 1.17 9 3.09 2.39 1.86 1.66 3.33 2.45 2.65 1.78 1.78 1.00 3.14 2.56 1.88 1.75 3.38 2.61 2.84 2.01 1.17 3.22 2.67 1.89 1.82 3.46 2.85 2.96 2.22 1.2 3.28 2.94 1.95 1.94 3.70 2.95 3.27 2.67 1.3 3.83 3.32 3.14 2.11 3.78 3.03 3.28 2.86 1.4 3.95 3.60 3.35 2.12 3.90 3.05 3.34 3.11 1.5 4.17 3.69 3.38 2.34 3.97 3.08 4.17 3.69 3.88 2.34 3.97 3.08 4.17 3.69 3.88 2.34 3.97 3.08 4.17 3.19 1.6 4.42 3.80 3.65 2.59 3.99 3.36 4.53 3.86 1.7 4.61 3.87 3.73 2.70 4.06 3.41 4.59 4.91 1.8 6.44 4.74 3.77 2.88 4.65 3.43 5.00 5.13 1.9 6.66 4.92 4.07 3.01 4.79 3.47 5.08 5.20 2.0 7.00 5.21 4.21 3.02 5.09 3.48 5.74 5.56 2.1 4.21 3.02 5.09 3.48 5.74 5.56 2.1 7.01 5.66 4.70 3.26 5.18 3.54 6.00 5.69 2.2 7.05 5.85 4.84 3.31 5.22 3.67 6.09 5.95 2.23 7.17 6.07 5.13 3.46 5.63 3.71 6.27 5.97 2.4 7.24 6.37 5.25 3.56 5.98 3.73 6.52 6.39 2.5 7.26 6.40 5.26 4.01 6.02 3.84 6.72 6.46 2.26 7.88 6.62 5.55 4.15 6.24 3.94 6.97 6.69 2.2 7.05 8.85 7.26 6.40 5.26 4.01 6.02 3.84 6.72 6.46 2.26 7.88 6.62 5.55 4.15 6.24 3.94 6.97 6.69 3.2 3 1.0 2.2 3.0 3.1 6.36 6.21 6.51 4.11 9.01 7.13 2.9 8.45 7.35 7.52 6.35 6.69 4.54 9.2 3.9 9.13 7.41 7.69 6.85 6.73 4.90 9.30 7.63 3.1 1.99 8.85 7.35 7.52 6.35 6.69 4.59 9.78 7.59 3.35 1.14 1.19 9.8 8.05 7.71 7.06 8.25 6.19 9.78 7.99 3.2 1.01 8.14 7.75 7.75 9.35 6.71 9.82 7.95 3.3 10.60 9.29 8.01 7.82 9.41 6.94 11.01 8.25 3.3 10.60 9.29 8.01 7.82 9.41 6.94 11.01 8.25 3.3 10.60 9.29 8.01 7.82 9.41 6.94 11.01 8.25 4.40 11.01 8.25 4.40 11.01 8.25 4.40 11.01 8.25 4.40 11.01 8.25 4.40 11.01 8.25 6.69 4.40 11.02 8.14 11.19 8.16 8.86 8.86 11.65 11.21 8.53 8.99 11.04 9.01 15.48 8.86 11.65 11.21 8.53 8.99 11.04 9.01 15.48 8.86 3.99 11.04 9.01 15.48 8.86 4.99 3.06 3.06 3.06 3.06 3.06 3.06 3.06 3.06	6									2.
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35										9
36       11.65       11.21       8.53       8.99       11.04       9.01       15.48       8.86         37       13.32       12.26       10.90       9.67       12.14       9.99       17.63       11.56         38       14.58       12.81       10.99       10.30       12.85       11.65       19.18       13.00         39       15.51       13.59       14.91       11.92       13.76       12.65       20.12       14.92         40       17.01       15.33       19.41       14.55       17.44       13.68       20.36       15.90         41       19.12       16.15       21.25       14.96       18.30       16.73       22.57       16.12         42       21.41       16.30       26.97       17.49       23.77       18.17       31.59       16.33         43       27.59       16.39       36.55       19.88       30.64       18.42       32.37       26.89         44       17.99       38.65       21.45       32.87       19.07       42.23       29.01         45       22.36       15.822       18.06       13.761       17.956       15.51       21.686       39.49 <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<>										
13.32   12.26   10.90   9.67   12.14   9.99   17.63   11.56     38										
38       14.58       12.81       10.99       10.30       12.85       11.65       19.18       13.00         39       15.51       13.59       14.91       11.92       13.76       12.65       20.12       14.92         40       17.01       15.33       19.41       14.55       17.44       13.68       20.36       15.90         41       19.12       16.15       21.25       14.96       18.30       16.73       22.57       16.12         42       21.41       16.30       26.97       17.49       23.77       18.17       31.59       16.33         43       27.59       16.39       36.55       19.88       30.64       18.42       32.37       26.89         44       17.99       38.65       21.45       32.87       19.07       42.23       29.01         45       22.36       36.67       23.97       46.46       33.26         39.49         4h percentile       15.324       15.822       18.06       13.761       17.956       15.51       21.686       16.225         4h percentile       2.234       1.612       1.229       1.386       2.966       1.332       1.612       0.565										1
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43 27.59 16.39 36.55 19.88 30.64 18.42 32.37 26.89 17.99 38.65 21.45 32.87 19.07 42.23 29.01 36.67 23.97 46.46 33.26 39.49 th percentile the percentile 2.234 1.612 1.229 1.386 2.966 1.332 1.612 0.565						1	1			20
44     17.99     38.65     21.45     32.87     19.07     42.23     29.01       45     22.36     22.36     36.67     23.97     46.46     33.26       39.49       21.45     15.324     15.822     18.06     13.761     17.956     15.51     21.686     16.225       22.34     1.612     1.229     1.386     2.966     1.332     1.612     0.565						I		1		22
45 46 22.36 36.67 23.97 46.46 33.26 39.49 th percentile 15.324 15.822 18.06 13.761 17.956 15.51 21.686 16.225 th percentile 2.234 1.612 1.229 1.386 2.966 1.332 1.612 0.565		27.00				l .	1	1		22
46     39.49       th percentile th percentile     15.324   15.822   18.06   13.761   17.956   15.51   21.686   16.225   1.386   2.966   1.332   1.612   0.565   1.332   0.565   1.332   0.565   1.332   0.565   1.332   0.565   1.332   0.565   1.332   0.565   0.56							1	I .	33.26	34
th percentile 2.234 1.612 1.229 1.386 2.966 1.332 1.612 0.565									39.49	
th percentile 2.234 1.612 1.229 1.386 2.966 1.332 1.612 0.565	th percentile	15.324	15.822	18.06	13.761	17.956	15.51	21.686		
40.40 40.00 47.00 47.01						2,966	1.332	1.612	0.565	2.0
year average 90th percentile   15.74   16.40   16.32   17.23   17.84	ear average 90	th percent	tile	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	15.74	16.40	16.32	17.23	17.84	17

	Coal Fossil Units 3 NERC Data	00-399 <b>MW</b>								
1		1999	2000	2001						2007
1   1.33	1									0.13 0.77
4 1.44 0.67 0.51 0.67 0.79 0.79 0.89 1.73 0.94 0.85 1.44 1.00 0.68 0.55 0.73 0.84 0.85 1.44 1.00 0.68 0.67 0.44 1.01 0.85 1.13 1.00 0.84 0.85 1.44 1.00 0.68 0.67 0.44 1.01 0.85 1.13 1.00 0.85 1.14 1.00 0.85 1.14 1.00 0.85 1.13 1.10 0.85 1.13 1.10 0.85 1.10	2									0.82
5							0.69	1.13		0.84
8 1 84 1 25 079 0.51 1.09 1.03 1.45 1.22 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.38 1.29 1.39 1.39 1.39 1.39 1.39 1.39 1.39 1.3	5									0.89
8										1.19 1.23
1   186										1.83
10										1.91
122 2.42 1.38 1.28 0.75 1.65 1.47 2.12 1.48 1.32 2.71 1.57 1.29 0.87 1.79 1.63 2.15 1.76 1.44 2.93 2.01 1.31 0.88 1.94 1.72 2.56 1.194 1.57 1.32 2.55 2.30 1.36 0.92 2.22 2.14 2.75 1.96 1.96 1.96 1.96 1.96 1.96 1.96 1.96				0.98						2.06
10										2.07 2.30
14										2.34
16										2.37
17   3.28   2.51   1.57   0.98   2.38   2.25   2.90   2.16   18   3.43   2.56   1.74   0.99   2.40   2.20   3.05   2.28   19   3.88   2.60   1.77   1.09   2.55   2.33   3.11   2.28   2.29   2.40   2.55   2.31   3.11   2.28   2.29   2.40   2.55   2.31   3.11   2.28   2.29   2.40   2.40   2.55   2.31   3.11   2.28   2.29   2.40				1.36						2.40
18										2.49 2.59
19   3.58   2.60   1.77   1.09   2.55   2.33   3.11   2.28   2.10   2.11   2.										2.66
20   3.92   2.79   1.84   1.13   2.66   2.60   3.15   2.31										2.70
21										2.84
22		4.05								2.94 3.02
24 4.31 3.09 2.07 1.26 3.06 3.06 3.86 2.83 2.83 2.99 1.30 3.23 3.16 3.89 3.02 2.86 4.40 3.35 2.10 1.31 3.78 3.19 3.97 3.14 2.77 4.54 3.49 2.28 1.52 3.89 3.23 3.98 3.21 3.34 2.29 4.66 4.20 2.57 1.82 4.06 3.72 4.64 3.65 3.04 8.0 4.35 2.62 2.39 4.10 3.73 4.86 3.71 3.1 4.84 4.63 2.71 2.42 4.24 3.83 3.49 4.00 3.21 4.84 4.63 2.71 2.42 4.24 3.83 4.93 4.00 3.21 4.94 4.67 2.72 2.58 4.38 4.04 5.01 4.01 3.23 4.94 4.67 2.72 2.58 4.38 4.04 4.07 5.38 4.09 3.09 4.00 3.25 4.94 4.67 3.25 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.25 5.22 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.65 5.52 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.66 5.56 5.01 3.36 3.34 4.93 5.93 6.15 5.80 5.70 3.40 3.34 3.49 3.59 6.15 5.80 5.70 3.40 3.36 3.34 4.93 5.80 5.70 3.40 3.36 3.64 5.02 5.86 6.33 5.57 4.91 3.29 3.99 4.83 4.86 4.91 5.86 4.94 4.67 5.83 5.80 5.70 3.40 3.36 3.64 5.02 5.86 6.33 5.57 4.91 3.29 3.99 5.83 5.90 3.46 3.84 4.91 5.26 5.97 5.12 4.91 3.29 3.99 4.83 4.86 4.91 5.86 4.94 4.91 5.86 6.44 3.55 5.90 5.90 5.83 5.90 3.46 3.84 4.91 5.26 5.97 5.12 4.91 3.29 3.99 4.83 4.86 4.91 5.86 6.35 5.76 6.11 3.36 3.44 3.49 3.59 5.80 5.70 3.40 3.45 3.64 5.02 5.86 5.97 5.12 4.91 3.29 3.99 4.83 4.86 6.33 5.57 6.11 5.80 6.95 6.84 4.91 5.86 6.24 4.25 5.25 5.77 6.71 5.81 4.26 6.66 6.46 3.74 4.77 5.31 5.78 7.06 5.99 8.18 4.91 5.78 7.06 5.99 8.18 4.91 5.78 7.06 5.99 8.18 4.91 5.78 7.06 5.99 8.18 6.83 5.77 6.71 5.81 4.91 5.78 7.06 5.99 8.18 8.81 7.62 5.80 5.92 5.93 5.94 5.99 8.18 6.83 5.77 6.71 5.81 5.90 8.09 6.76 6.95 5.95 5.93 6.38 6.43 8.37 7.18 8.77 7.82 6.69 5.64 6.65 7.76 7.19 9.47 8.83 8.81 7.69 5.95 5.83 6.38 5.20 5.20 5.88 8.33 7.04 4.91 5.25 5.90 5.90 8.09 6.76 6.95 5.90 5.90 5.90 5.90 5.90 5.90 5.90 5										3.02
25										3.10
1.56							3.16	3.89	3.02	3.31
28	26	4.40	3.35	2.10	1.31					3.42
29										3.76 4.05
30										4.20
31								4.86		4.31
33 5.00 4.77 2.79 2.59 4.41 4.27 5.38 4.19 3.4 5.07 4.89 2.89 2.96 4.65 4.32 5.40 4.21 3.29 3.69 4.65 4.32 5.40 4.21 3.36 5.52 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.69 3.60 5.56 5.01 3.36 3.13 4.86 4.91 5.86 4.94 3.57 5.75 5.29 3.37 3.41 4.91 5.26 5.97 5.12 3.8 5.80 5.70 3.40 3.43 4.93 5.99 6.15 5.34 3.9 5.83 5.90 3.46 3.64 5.02 5.48 6.33 5.57 4.0 6.09 6.14 3.55 4.20 5.05 5.69 6.63 5.76 4.1 6.36 6.24 3.62 4.25 5.25 5.77 6.71 5.81 4.2 6.66 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.3 7.30 6.86 3.32 4.68 5.38 5.52 7.28 6.28 4.4 7.38 6.95 3.98 4.69 5.45 5.88 7.53 6.75 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.		4.84	4.63	2.71						4.73
34 5.07 4.89 2.99 2.98 4.66 4.32 5.40 4.21 3.55 5.22 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.66 5.66 5.01 3.29 3.09 4.83 4.66 5.71 4.91 3.66 5.66 5.01 3.36 3.13 4.86 4.91 5.26 5.97 5.12 3.8 5.80 5.70 3.40 3.43 4.91 5.26 5.97 5.12 3.8 5.80 5.70 3.40 3.43 4.93 5.99 6.15 5.34 4.91 6.36 6.24 3.66 4.20 5.05 5.69 6.63 5.76 4.20 5.05 5.69 6.63 5.76 4.20 5.05 5.29 6.67 6.71 5.81 4.20 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.20 5.05 5.25 5.77 6.71 5.81 4.20 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.25 5.25 5.77 6.71 5.81 4.20 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.69 5.45 5.88 7.53 6.75 6.75 6.75 6.75 6.75 6.75 6.75 6.75										5.05 5.20
35 5.22 4.91 3.29 3.09 4.83 4.66 5.71 4.91 3.66 5.57 5.29 3.37 3.41 4.91 5.26 5.97 5.12 3.86 5.57 5.29 3.37 3.41 4.91 5.26 5.97 5.12 3.88 5.80 5.70 3.40 3.43 4.93 5.99 6.15 5.34 3.95 5.90 3.46 3.64 4.93 5.99 6.15 5.34 3.95 5.90 3.46 3.64 4.20 5.05 5.69 6.63 5.76 4.10 6.09 6.14 3.55 4.20 5.05 5.69 6.63 5.76 4.10 6.66 6.64 6.66 6.64 3.74 4.47 5.31 5.78 7.06 5.89 4.10 5.10 5.78 7.06 5.89 4.10 5.10 5.78 7.06 5.89 5.10 5.10 5.10 5.10 5.10 5.10 5.10 5.10										5.26
36			1	1					4.91	5.39
38 5.80 5.70 3.40 3.43 4.93 5.39 6.15 5.34 5.57 4.00 6.09 6.14 3.55 4.20 5.05 5.69 6.63 5.76 6.63 5.76 4.0 6.09 6.14 3.55 4.20 5.05 5.69 6.63 5.76 6.63 5.76 4.1 6.36 6.24 3.62 4.25 5.25 5.77 6.71 5.81 4.2 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.20 6.66 6.46 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.20 6.66 6.46 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.20 6.66 6.46 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.20 6.28 4.47 7.38 6.95 3.98 4.69 5.45 5.88 7.53 6.75 6.76 4.5 7.63 7.07 5.24 4.97 5.51 5.90 8.09 6.76 4.5 7.63 7.07 5.24 4.97 5.51 5.90 8.09 6.76 6.13 8.18 6.83 4.7 8.15 7.43 5.77 5.29 6.07 6.11 8.27 6.95 4.8 8.18 7.62 5.80 5.32 6.23 6.38 8.33 7.04 4.9 8.39 7.69 5.95 5.38 6.38 6.43 8.37 7.18 5.0 8.41 7.72 6.15 5.42 6.48 6.45 8.50 8.03 5.1 8.77 7.82 6.69 5.64 6.96 7.02 8.69 8.26 5.2 9.06 8.02 6.72 6.05 7.38 7.11 9.41 8.32 5.3 9.43 8.61 6.85 6.40 7.50 7.18 9.47 8.34 5.4 9.62 9.10 7.36 6.57 7.61 7.39 9.56 8.76 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 10.79 11.70 8.85 7.09 8.78 8.29 10.52 8.90 10.52 8.90 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 6.1 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 11.65 8.31 6.76 6.85 4.96 9.72 9.57 11.59 9.50 11.70 8.85 7.09 8.78 8.29 10.52 8.90 10.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 9.50 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 9.90 9.70 9.72 9.57 11.59 9.50 11.65 8.31 6.76 8.74 7.63 10.43 8.86 6.1 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 11.59 9.50 11.64 8.95 11.25 12.33 18.00 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 9.50 11.25 9.89 11.43 12.15 8.89 8.99 8.84 9.16 10.68 9.13 11.02 9.60 12.57 13.83 16.01 12.05 13.69 16.27 2.20 13.18 12.25 13.89 16.01 17.74 17.99 13.63 11.65 11.60			5.01	3.36						5.55
39 5.83 5.90 3.46 3.64 5.02 5.48 6.33 5.57 6.40 6.09 6.14 3.55 4.20 5.05 5.69 6.63 5.76 6.71 5.81 4.20 6.66 6.46 3.74 4.47 5.31 5.78 7.06 5.89 4.3 7.30 6.86 3.82 4.68 5.38 5.82 7.28 6.28 4.47 5.31 5.78 7.06 6.95 3.99 4.69 5.45 5.88 7.53 6.75 6.75 4.50 6.75 4.50 6.75 6.70 5.24 4.97 5.51 5.90 8.09 6.76 4.66 7.68 7.15 5.53 5.23 5.94 5.99 8.18 6.83 4.7 8.15 7.43 5.77 5.29 6.07 6.11 8.27 6.95 6.23 6.38 8.33 7.04 4.99 8.39 7.69 5.95 5.38 6.23 6.38 8.33 7.04 4.99 8.39 7.69 5.95 5.38 6.38 6.43 8.37 7.18 5.50 8.41 7.72 6.15 5.95 5.34 6.38 6.43 8.37 7.18 5.50 8.41 7.72 6.15 5.42 6.69 6.48 6.45 8.50 8.03 5.1 8.77 7.82 6.69 5.64 6.96 7.02 8.69 8.26 5.29 9.06 8.02 6.72 6.05 7.38 7.11 9.41 8.32 5.3 9.43 8.61 6.86 6.40 7.50 7.18 9.47 8.34 5.4 9.62 9.10 7.36 6.57 7.61 7.39 9.56 8.76 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 6.00 10.70 9.17 0.9 11.40 10.70 8.86 7.09 8.78 8.29 10.52 8.90 10.52 8.9				1						5.69 5.82
10		1	1	1						5.85
41				1						5.90
43 7.30 6.86 3.82 4.68 5.38 5.82 7.28 6.28 4.4 7.38 6.95 3.98 4.69 5.45 5.88 7.53 6.75 4.5 7.63 7.07 5.24 4.97 5.51 5.90 8.09 6.76 6.76 7.68 7.15 5.53 5.23 5.94 5.99 8.18 6.83 4.7 8.15 7.43 5.77 5.29 6.07 6.11 8.27 6.95 4.99 8.39 7.69 5.95 5.38 6.38 6.43 8.37 7.18 6.95 6.95 6.95 6.95 6.95 6.95 6.95 6.95			6.24							6.01
44 7,38 6,95 3,98 4,69 5,45 5,88 7,53 6,75 4,676 4,67 7,68 7,15 5,53 5,23 5,94 5,99 8,18 6,83 4,7 8,15 7,43 5,77 5,29 6,07 6,11 8,27 6,95 8,18 8,18 7,62 5,80 5,32 6,23 6,38 8,33 7,04 8,18 5,00 8,41 7,72 6,15 5,42 6,48 6,45 8,50 8,03 5,1 8,77 7,82 6,69 5,64 6,96 7,02 8,69 8,26 5,2 9,06 8,02 6,72 6,05 7,38 7,11 9,41 8,32 5,3 9,43 8,61 6,85 6,40 7,50 7,18 9,47 8,34 5,4 9,62 9,10 7,36 6,57 7,61 7,39 9,56 8,76 5,10,29 9,49 7,64 6,63 8,13 7,45 10,00 8,77 5,61 10,35 11,65 8,31 6,76 8,74 7,63 10,43 8,86 15,7 10,79 11,70 8,85 7,09 8,78 8,29 10,52 8,90 11,12 12,13 8,87 7,21 8,80 8,46 10,67 9,03 5,9 11,43 12,15 8,89 8,09 8,84 9,16 10,68 9,13 6,1 12,06 15,61 9,90 9,00 9,72 9,57 11,14 9,49 11,20 9,49 11,20 9,40 11,20 11,20 9,40 11,20 11,20 9,40 11,20 11,20 9,40 11,20 11,20 11,20 11,20 11,20 11,20 11,20 11			1							6.62 6.73
1.00		l .		1	1					6.78
46				1	1		5.90			7.19
48 8.18 7.62 5.80 5.32 6.23 6.38 8.33 7.04 49 8.39 7.69 5.95 5.38 6.38 6.43 8.37 7.18 5.0 8.41 7.72 6.15 5.42 6.48 6.45 8.50 8.03 5.1 8.77 7.82 6.69 5.64 6.96 7.02 8.69 8.26 5.2 9.06 8.02 6.72 6.05 7.38 7.11 9.41 8.32 5.3 9.43 8.61 6.85 6.40 7.50 7.18 9.47 8.34 9.62 9.10 7.36 6.57 7.61 7.39 9.56 8.76 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.79 11.70 8.85 7.09 8.78 8.29 10.52 8.90 11.70 8.85 7.09 8.78 8.29 10.52 8.90 11.43 12.15 8.89 8.09 8.84 9.16 10.67 9.03 5.9 11.43 12.15 8.89 8.09 8.84 9.16 10.67 9.03 6.1 1.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 9.16 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 6.2 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 6.3 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 6.4 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 17.44 13.61 6.6 13.89 62.44 10.68 12.10 10.74 17.99 13.63 11.21 12.20 13.18 26.20 14.62 12.55 12.38 16.01 17.09 13.63 17.09 1		1	7.15	1						7.23
49   8.99   7.69   5.95   5.38   6.38   6.43   8.37   7.18		1			1		1			7.37 7.67
50 8.41 7.72 6.15 5.42 6.48 6.45 8.50 8.03 51 8.77 7.82 6.69 5.64 6.96 7.02 8.69 8.26 52 9.06 8.02 6.72 6.05 7.38 7.11 9.41 8.32 53 9.43 8.61 6.85 6.40 7.50 7.18 9.47 8.34 9.62 9.10 7.36 6.57 7.61 7.39 9.56 8.76 55 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 56 10.35 11.65 8.31 6.76 8.74 7.63 10.43 8.86 57 10.79 11.70 8.85 7.09 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.78 8.29 10.52 8.90 8.70 8.70 8.70 8.70 8.70 8.70 8.70 8.7		1		1						7.68
51         8.77         7.82         6.69         5.64         6.96         7.02         8.69         8.26           52         9.06         8.02         6.72         6.05         7.38         7.11         9.41         8.32           53         9.43         8.61         6.85         6.40         7.50         7.18         9.47         8.34           54         9.62         9.10         7.36         6.57         7.61         7.39         9.56         8.76           55         10.29         9.49         7.64         6.63         8.13         7.45         10.00         8.77           56         10.35         11.65         8.31         6.76         8.74         7.63         10.43         8.86           57         10.79         11.70         8.85         7.02         8.80         8.46         10.67         9.03           58         11.12         12.13         8.87         7.21         8.80         8.46         10.67         9.03           59         11.43         12.15         8.89         8.09         8.84         9.16         10.68         9.13           61         12.06         15.61         9.90 <td></td> <td></td> <td></td> <td>1</td> <td>i .</td> <td></td> <td></td> <td></td> <td></td> <td>7.80</td>				1	i .					7.80
53 9.43 8.61 6.85 6.40 7.50 7.18 9.47 8.34 9.62 9.10 7.36 6.57 7.61 7.39 9.56 8.76 5.5 10.29 9.49 7.64 6.63 8.13 7.45 10.00 8.77 5.5 10.35 11.65 8.31 6.76 8.74 7.63 10.43 8.86 5.7 10.79 11.70 8.85 7.09 8.78 8.29 10.52 8.90 5.5 11.12 12.13 8.87 7.21 8.80 8.46 10.67 9.03 5.9 11.43 12.15 8.89 8.09 8.84 9.16 10.68 9.13 6.0 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 6.1 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 6.2 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 6.3 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 6.4 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 6.5 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 6.6 13.89 6.2.44 10.68 12.52 12.35 10.68 14.56 13.89 6.2.44 10.68 12.50 13.69 16.27 20.59 11.69 14.86 14.56 14.86 14.56 15.09 70 15.09 71 16.30 72 17.06 73 17.48 74 18.40 10.09 10.68 9.98 10.55 11.32 11.17 10th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21			7.82	6.69						8.18
54         9.62         9.10         7.36         6.57         7.61         7.39         9.56         8.76           55         10.29         9.49         7.64         6.63         8.13         7.45         10.00         8.77           56         10.35         11.65         8.31         6.6         8.74         7.63         10.43         8.86           57         10.79         11.70         8.85         7.09         8.78         8.29         10.52         8.90           58         11.12         12.13         8.87         7.21         8.80         8.46         10.67         9.03           59         11.43         12.15         8.89         8.09         8.84         9.16         10.68         9.13           60         11.72         13.38         9.60         8.91         9.06         9.27         11.14         9.49           61         12.06         15.61         9.90         9.00         9.72         9.57         11.59         9.50           62         12.39         15.97         10.18         9.43         11.02         9.60         12.57         10.83           63         12.66         16.71         <		1								8.21 8.24
10.29   9.49   7.64   6.63   8.13   7.45   10.00   8.77			1	1						8.75
56 10.35 11.65 8.31 6.76 8.74 7.63 10.43 8.86 57 10.79 11.70 8.85 7.99 8.78 8.29 10.52 8.90 58 11.12 12.13 8.87 7.21 8.80 8.46 10.67 9.03 59 11.43 12.15 8.89 8.09 8.84 9.16 10.68 9.13 60 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 61 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 62 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 63 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 64 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 65 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 16.66 13.89 62.44 11.21 12.20 13.18 26.20 14.62 68 14.56 69 14.86 14.56 69 14.86 16.50 12.55 12.38 16.01 17.09 15.09 70 15.09 71 16.30 72 17.06 73 17.48 74 18.40 90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 1.00 1.00 10.00 10.00 10.00 11.00			1		1		1	10.00	8.77	8.83
58         11.12         12.13         8.87         7.21         8.80         8.46         10.67         9.03           59         11.43         12.15         8.89         8.09         8.84         9.16         10.68         9.13           60         11.72         13.38         9.60         8.91         9.06         9.27         11.14         9.49           61         12.06         15.61         9.90         9.00         9.72         9.57         11.59         9.50           62         12.39         15.97         10.18         9.43         11.02         9.60         12.57         10.83           63         12.66         16.71         12.09         9.70         11.25         9.89         16.46         12.52           64         13.18         29.54         15.06         9.85         11.28         10.08         16.90         13.29           65         13.57         37.72         16.48         9.97         11.47         10.29         17.44         13.61           66         13.89         62.44         10.68         12.10         10.74         17.99         13.63           67         14.99         84.85 <td< td=""><td></td><td>10.35</td><td>11.65</td><td>8.31</td><td>6.76</td><td></td><td></td><td></td><td></td><td>9.44</td></td<>		10.35	11.65	8.31	6.76					9.44
11.43   12.15   8.89   8.09   8.84   9.16   10.68   9.13	57	10.79								9.64 10.42
60 11.72 13.38 9.60 8.91 9.06 9.27 11.14 9.49 61 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 62 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 63 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 64 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 65 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 16.66 13.89 62.44 10.68 12.10 10.74 17.99 13.63 67 14.19 84.85 11.21 12.20 13.18 26.20 14.62 68 14.56 12.55 12.38 16.01 17.09 69 14.86 14.56 12.55 12.38 16.01 17.09 69 14.86 26.20 17.06 73 17.48 74 18.40 20.59 18.96 26.22 31.57 36.81 79 18.40 20.59 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21 4.21 4.21 4.21 4.21 4.21 4.21 4.21			1			1	ł			11.17
61 12.06 15.61 9.90 9.00 9.72 9.57 11.59 9.50 62 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 63 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 64 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 65 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 66 13.89 62.44 67 14.19 84.85 11.21 12.20 13.18 26.20 14.62 13.69 69 14.86 70 15.09 69 14.86 70 15.09 71 16.30 70 15.09 71 16.30 71 16.30 72 17.06 73 17.48 74 18.40 90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21	ł .	1		1				11.14	9.49	11.75
62 12.39 15.97 10.18 9.43 11.02 9.60 12.57 10.83 12.66 16.71 12.09 9.70 11.25 9.89 16.46 12.52 64 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 17.44 13.61 66 13.89 62.44 10.68 12.10 10.74 17.99 13.63 67 14.19 84.85 11.21 12.20 13.18 26.20 14.62 68 14.56 69 14.86 70 15.09 70 15.09 71 16.30 72 17.06 73 17.48 74 18.40 20.59 20.50 20.50 20.50 20.50 20.50 20.50 20.50 20.50		1	15.6	9.90	9.00	9.72	9.57			12.48
64 13.18 29.54 15.06 9.85 11.28 10.08 16.90 13.29 65 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 10.68 12.10 10.74 17.99 13.63 16.01 12.20 13.18 26.20 14.62 12.55 12.38 16.01 12.55 12.38 16.01 17.09 13.69 14.86 12.55 12.38 16.01 12.55 12.38 16.01 12.57 12.58 16.01 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 16.01 12.55 12.55 12.38 12.55 12.55 12.38 12.55 12.55 12.38 12.55 12.55 12.38 12.55 12.55 12.55 12.55 12.38 12.55 12	62	12.39	15.97	1	1					12.52 12.70
65 13.57 37.72 16.48 9.97 11.47 10.29 17.44 13.61 16.68 13.89 62.44 10.68 12.10 10.74 17.99 13.63 16.01 17.09 14.62 12.55 12.38 16.01 17.09 13.69 14.86 14.56 12.55 12.38 16.01 17.09 13.69 14.86 14.86 13.69 16.27 17.09 18.96 16.27 17.06 17.0		•		1	1					13.28
66 13.89 62.44 10.68 12.10 10.74 17.99 13.63 67 14.19 84.85 11.21 12.20 13.18 26.20 14.62 17.09 69 14.86 12.55 12.38 16.01 13.69 16.27 20.59 70 15.09 71 16.30 72 17.06 73 17.48 74 18.40 20.59		1	1		1				1	13.44
67 14.19 84.85 11.21 12.20 13.18 26.20 14.62 17.09 68 14.86 14.86 15.09 15.09 20.59 18.96 26.22 31.57 36.81 74 18.40 90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21			1	1		I .	10.74		ı	13.5
69 14.86 69 14.86 70 15.09 71 16.30 72 17.06 73 17.48 74 18.40 90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21	67	14.19	84.8	5				26.20		13.94 17.40
70 15.09 71 16.30 72 17.06 73 17.48 74 18.40  20th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21		1			12.55			1		17.40
71 16.30 72 17.06 73 17.48 74 18.40  90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21  4 year average 90th percentile 11.60 10.88 9.98 10.59 11.10		1				1		İ	20.55	19.30
72 17.06 73 17.48 74 18.40  90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21  4 year average 90th percentile 11.60 10.88 9.98 10.59 11.10					1		26.22	1		23.20
90th percentile 14.10 14.27 8.88 9.13 11.25 10.65 11.32 11.17 10th percentile 1.85 1.17 0.78 0.50 1.09 1.06 1.40 1.21 4 year average 90th percentile 11.60 10.88 9.98 10.59 11.10			1	1 .	1		1			29.4
90th percentile         14.10         14.27         8.88         9.13         11.25         10.65         11.32         11.17           10th percentile         1.85         1.17         0.78         0.50         1.09         1.06         1.40         1.21           4 year average 90th percentile         11.60         10.88         9.98         10.59         11.10	73	17.48	1				36.81		l	59.75 66.77
90th percentile         14.10         1.21           10th percentile         1.85         1.17         0.78         0.50         1.09         1.06         1.40         1.21           4 year average 90th percentile         11.60         10.88         9.98         10.59         11.10	74	18.40	יי							
10th percentile         1.85         1.17         0.78         0.50         1.09         1.06         1.40         1.21           4 year average 90th percentile         11.60         10.88         9.98         10.59         11.10	90th percentile									13.8
4 year average sour percentile		1.8	5 1.1	7] 0.78	0.50	1.09	1.06	1.40	1.21	1.8
	4 year average 90	th percent	ile	No.						
4 year average 10th percentile   1.07   0.88   0.86   1.01   1.19	4 year average 10	th percent	ile	100	1.07	0.88	0.86	1.01	1.19	1.38



NERC Industry data distribution curve, 600-699 MW, 1999



**Normal Distribution or Bell Curve** 

#### The Normal Distribution curve shows the following:

The mean is the  $\mu$  symbol and a standard deviation is the  $\sigma$  symbol. 68 % of the values fall within 1 standard deviation of the mean. 95% of the values fall within 2 standard deviations of the mean. 99.7% of the variables fall within 3 standard deviations of the mean. less than 1% of the variables falling outside 3 standard deviations from the mean.

# By comparison, the NERC distribution curve, above, of the 1999 forced outage rates shows:

Where the mean = 6.5 and the std dev = 4.6

75% of the values fall within 1 standard deviation, the value will be less than 11.1, or greater than 1.9. 95% of the values fall within 2 standard deviations, the value will be less than 15.7 or greater than -2.7 100% of the values fall within 3 standard deviations, the value will be less than 20.3 However, as you can see these are not equally distributed on both sides of the mean.

# **CERTIFICATE OF SERVICE**

## **UM 1355**

I certify that I have this day served the foregoing document upon all parties of record in this proceeding by delivering a copy in person or by mailing a copy properly addressed with first class postage prepaid, or by electronic mail pursuant to OAR 860-13-0070, to the following parties or attorneys of parties.

Dated at Salem, Oregon, this 7th day of April, 2009.

Kay Barnes

**Public Utility Commission** 

**Regulatory Operations** 

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Telephone: (503) 378-5763

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